# **MDC5000T1**

# SMALLBLOCK™ Low Voltage Bias Stabilizer

- Maintains Stable Bias Current in Various Discrete Bipolar Junction and Field Effect Transistors
- Provides Stable Bias Using a Single Component Without Use of Emitter Ballast and Bypass Components
- Operates Over a Wide Range of Supply Voltages Down to 1.8 Vdc
- Reduces Bias Current Variation Due to Temperature and Unit-to-Unit Parametric Changes
- Consumes < 0.5 mW at V<sub>CC</sub> = 2.75 V

This device provides a reference voltage and acts as a DC feedback element around an external discrete, NPN BJT or N–Channel FET. It allows the external transistor to have its emitter/source directly grounded and still operate with a stable collector/drain DC current. It is primarily intended to stabilize the bias of discrete RF stages operating from a low voltage regulated supply, but can also be used to stabilize the bias current of any linear stage in order to eliminate emitter/source bypassing and achieve tighter bias regulation over temperature and unit variations. This device is intended to replace a circuit of three to six discrete components and is available in a SOT–143 package.

The combination of low supply voltage, low quiescent current drain, and small package make it ideal for portable communications applications such as:

- Cellular Telephones
- Pagers
- PCN/PCS Portables
- PCMCIA RF Modems
- Cordless Phones
- Broadband Transceivers and Other Portable Wireless Products

### MAXIMUM RATINGS

Rating	Symbol Value		Unit
Power Supply Voltage	VCC	15	Vdc
Ambient Operating Temperature Range	TA	-40 to +85	°C
Storage Temperature Range	T <sub>stg</sub>	-65 to +150	°C
Junction Temperature	Тј	150	°C
Collector Emitter Voltage (Q2)	V <sub>CEO</sub> –15		V

### THERMAL CHARACTERISTICS

Symbol	Max	Unit
PD	225	mW
	1.8	mW/∘C
R <sub>θJA</sub>	556	°C/W
	PD	PD 225

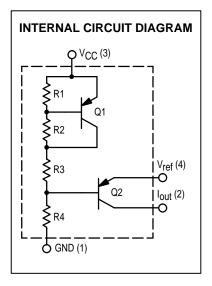
### DEVICE MARKING

MDC5000T1 = E5

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## MDC5000T1

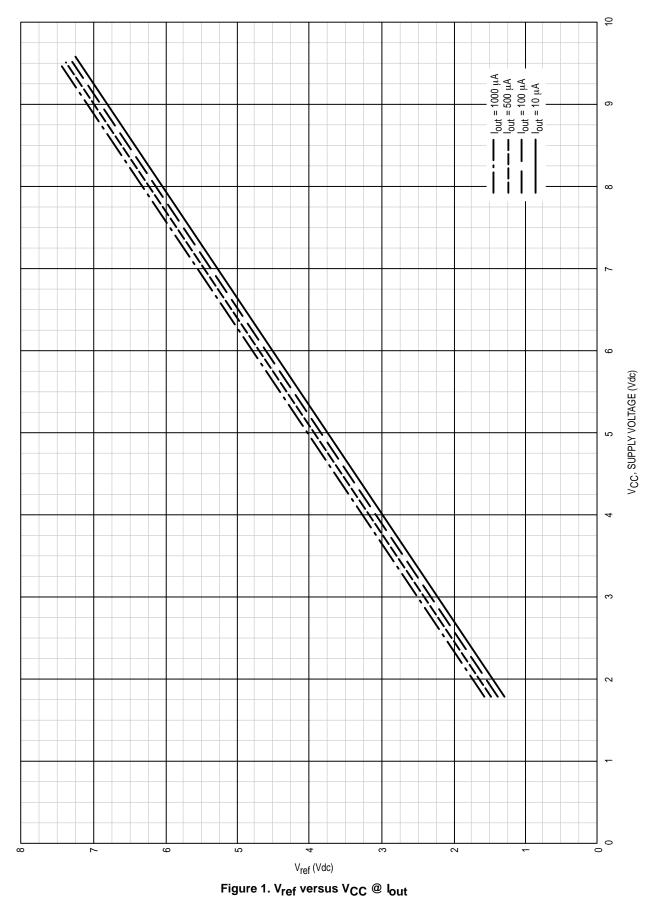
## **ELECTRICAL CHARACTERISTICS** (T<sub>A</sub> = $25^{\circ}$ C unless otherwise noted)

Characteristic	Symbol	Min	Тур	Max	Unit
Recommended Operating Supply Voltage	VCC	1.8	2.75	10	Volts
Power Supply Current (V <sub>CC</sub> = 2.75 V) V <sub>ref</sub> , I <sub>out</sub> are unterminated See Figure 8	ICC	—	110	200	μA
Q2 Collector Emitter Breakdown Voltage $(I_{C2} = 10 \ \mu A, I_{B2} = 0)$	V(BR)CEO2	-15			Volts
Reference Voltage (V <sub>CC</sub> = 2.75 V, V <sub>out</sub> = 0.7 V) ( $I_{out}$ = 30 $\mu$ A) ( $I_{out}$ = 150 $\mu$ A) See Figure 9	V <sub>ref</sub>	2.010 2.075	2.035 2.100	2.060 2.125	Volts
$ \begin{array}{l} \mbox{Reference Voltage} (V_{CC}=2.75 \ \mbox{V}, \ V_{out}=0.7 \ \mbox{V}, \ -40^{\circ}C \leq T_A \leq +85^{\circ}C) \\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	ΔV <sub>ref</sub>		±5 ±12 ±25	±10 ±25 ±50	mV

MDC5000T1

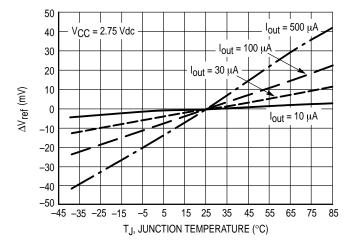
TYPICAL OPEN LOOP CHARACTERISTICS

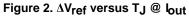
(Refer to Circuit of Figure 9)

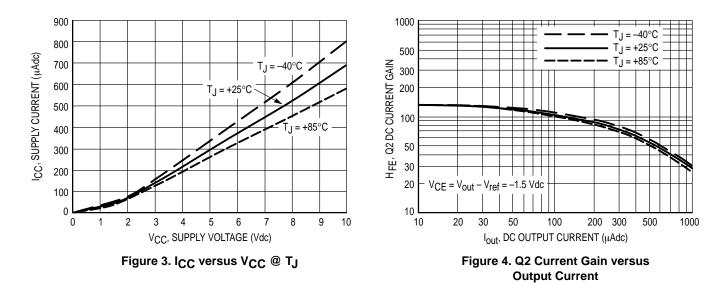


## **TYPICAL OPEN LOOP CHARACTERISTICS**

(Refer to Circuits of Figures 8, 10 & 11)







# TYPICAL CLOSED LOOP PERFORMANCE

(Refer to Circuits of Figures 12 & 13)

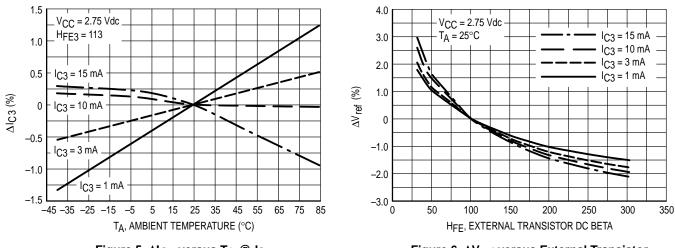


Figure 5.  $\Delta I_{C3}$  versus T<sub>A</sub> @ I<sub>C3</sub>

Figure 6.  $\Delta V_{ref}$  versus External Transistor DC Beta @ IC3

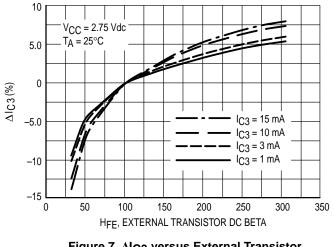
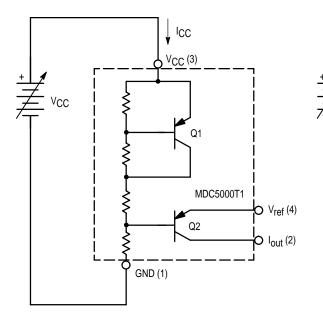
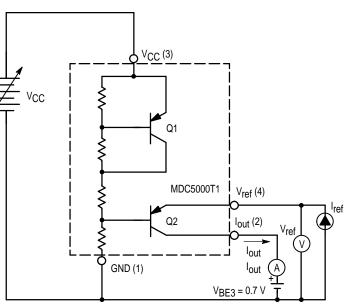


Figure 7.  $\Delta I_{C3}$  versus External Transistor DC Beta @ I<sub>C3</sub>

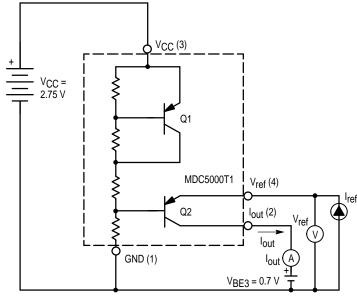
### **OPEN LOOP TEST CIRCUITS**

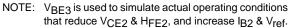




NOTE: V<sub>BE3</sub> is used to simulate actual operating conditions that reduce V<sub>CE2</sub> & H<sub>FE2</sub>, and increase I<sub>B2</sub> & V<sub>ref</sub>.

### Figure 9. Vref versus V<sub>CC</sub> Test Circuit







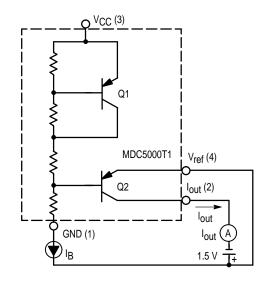


Figure 11. HFE versus Iout Test Circuit

Figure 8. ICC versus VCC Test Circuit

### **CLOSED LOOP TEST CIRCUITS**

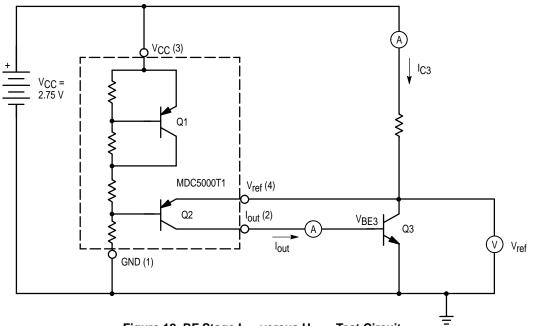


Figure 12. RF Stage IC3 versus HFE3 Test Circuit

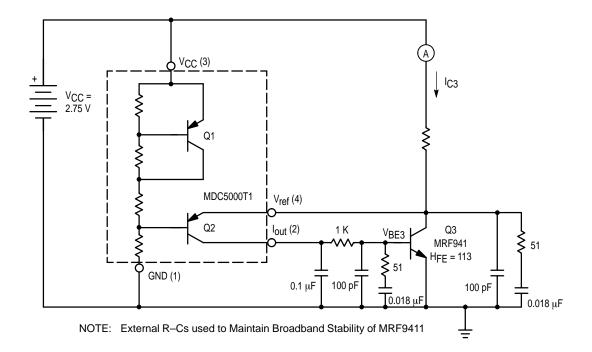
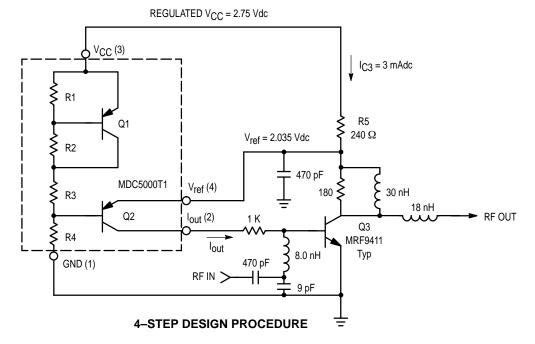
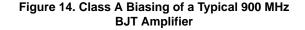
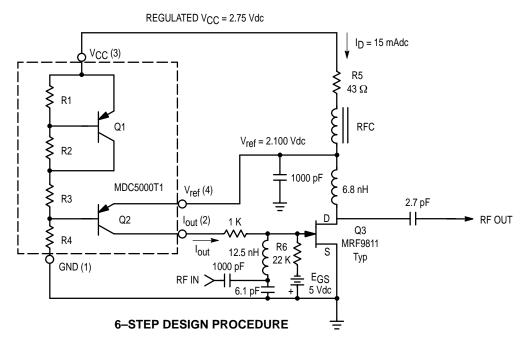


Figure 13. RF Stage  $I_{\mbox{C3}}$  versus  $T_{\mbox{A}}$  Test Circuit



- Step 1: Choose V<sub>CC</sub> (1.8 V Min to 10 V Max)
- Step 2: Choose bias current, IC3, and calculate needed Iout from typ HFE3
- Step 3: From Figure 1, read  $V_{ref}$  for  $V_{CC} \& I_{out}$  calculated.
- Step 4: Calculate Nominal R5 =  $(V_{CC} V_{ref}) \div (I_{C3} + I_{out})$ . Tweak as desired.



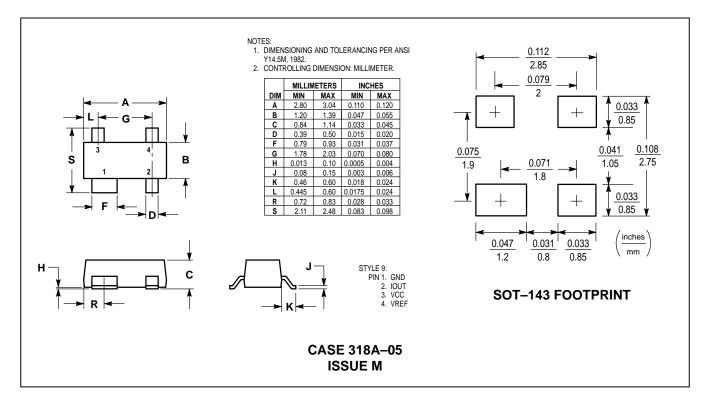


- Step 1: Choose V<sub>CC</sub> (1.8 V Min to 10 V Max)
- Step 2: Choose bias current, ID, and determine needed gate-source voltage, VGS.
- Step 3: Choose I<sub>out</sub> keeping in mind that too large an I<sub>out</sub> can impair MDC5000T1  $\Delta V_{ref}/\Delta T_J$  performance (Figure 2) but too large an R6 can cause I<sub>DGO</sub> & I<sub>GSO</sub> to bias on the FET.
- Step 4: Calculate R6 = (V<sub>GS</sub> + E<sub>GS</sub>)  $\div$  I<sub>out</sub>
- Step 5: From Figure 1, read V<sub>ref</sub> for V<sub>CC</sub> & I<sub>out</sub> chosen
- Step 6: Calculate Nominal R5 =  $(V_{CC} V_{ref}) \div (I_D + I_{out})$ . Tweak as desired.

#### Figure 15. Class A Biasing of a Typical 890 MHz Depletion Mode GaAs FET Amplifier

### **MDC5000T1**

### PACKAGE DIMENSIONS



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