CLC501 High-Speed Output Clamping Op Amp

General Description

The CLC501 is a high-speed current-feedback op amp with the unique feature of output voltage clamping. This feature allows both the maximum positive (Vhigh) and negative (Vlow) output voltage levels to be established. This is useful in a number of applications in which "downstream" circuitry must be protected from overdriving input signals. Not only can this prevent damage to downstream circuitry, but can also reduce time delays since saturation is avoided. The CLC501's very fast 1ns overload/clamping recovery time is useful in applications in which information-containing signals follow overdriving signals.

Engineers designing high-resolution, subranging A/D systems have long sought an amplifier capable of meeting the demanding requirements of the residue amplifier function. Amplifiers providing the residue function must not only settle quickly, but recover from overdrive quickly, protect the second stage A/D, and provide high fidelity at relatively high gain settings. The CLC501, which excels in these areas, is the ideal design solution in this onerous application. To further support this application, the CLC501 is both characterized and tested at a gain setting of +32—the most common gain setting for residue amplifier applications.

The CLC501's other features provide a quick, high-performance design solution. Since the CLC501's current feedback design requires no external compensation, designers need not spend their time designing compensation networks. The small 8-pin package and low, 180mW power consumption make the CLC501 ideal in numerous applications having small power and size budgets.

The CLC501 is available in several versions to meet a variety of requirements. A three-letter suffix determines the version:

CLC501AJP -40°C to +85°C 8-pin plastic DIP CLC501AJE -40°C to +85°C 8-pin plastic SOIC

DESC SMD number: 5962-89974

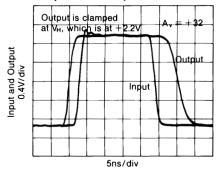
Features

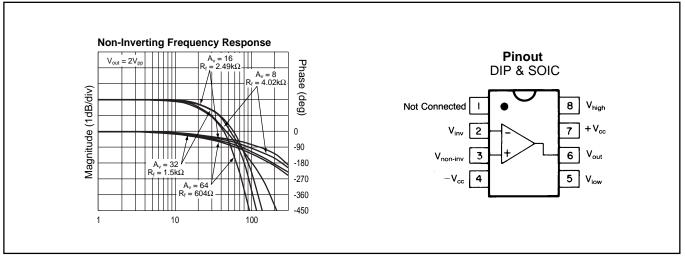
- Output clamping (V_{high} and V_{low})
- 1ns recovery from clamping/overdrive
- 0.05% settling in 12ns
- Characterized and guaranteed at $A_{v} = +32$
- Low power, 180mW

Applications

- Residue amplifier in high-accuracy, subranging A/D systems
- High-speed communications
- Output clamping applications
- Pulse amplitude modulation systems

Clamped Pulse Response



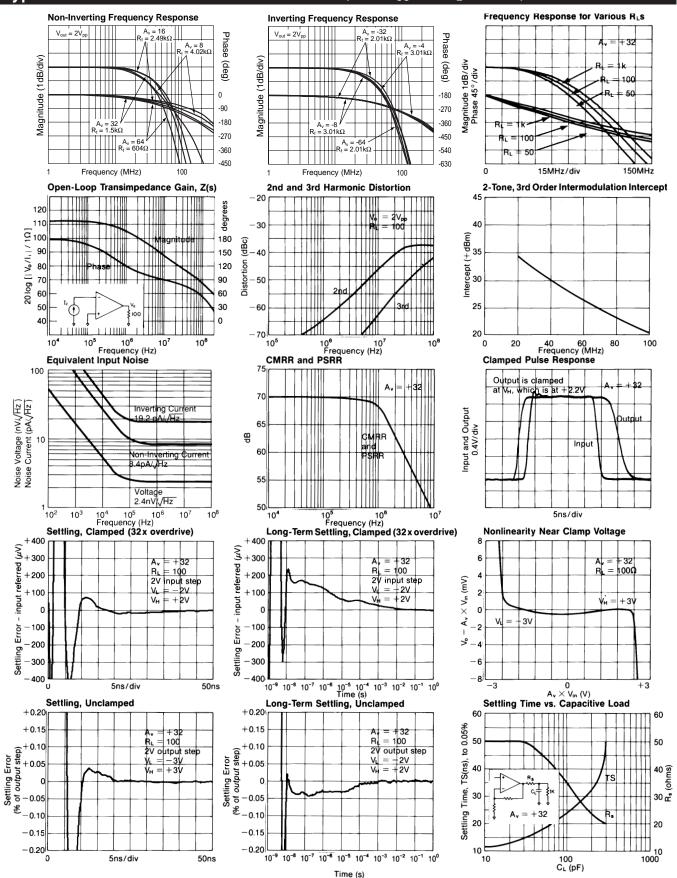


CLC501 Electrical	Characteristics	(A _V = +32,	V _{cc} = ±5V, R _l	= 100 Ω, R	= 1.5Ω, V _H =	= +3V; unless	specified)
PARAMETERS	CONDITIONS	TYP	MAX & MIN RATINGS			UNITS	SYMBOL
Ambient Temperature	CLC501AJ	+25°C	−40°C	+25°C	+85°C		
FREQUENCY DOMAIN PERFORMANCE							
-3dB bandwidth-3dB bandwidthgain flatness	$V_{\text{out}} < 5V_{\text{pp}}$ $@A_{\text{v}} = +20, V_{\text{out}} < 2V_{\text{pp}}$ $V_{\text{out}} < 5V_{\text{pp}}$	75 110	>60 >85	>60 >85	>45 >55	MHz MHz	SSBW SS20
peaking¹ peaking rolloff¹ linear phase deviation	<15MHz >15MHz <30MHz DC to 30MHz	0 0 0.2 0.2	<0.1 <0.2 <1.0 <1.0	<0.1 <0.2 <1.0 <1.0	<0.1 <0.2 <1.3 <1.0	dB dB dB °	GFPL GFPH GFR LPD
TIME DOMAIN PERFORMANCE							
rise and fall time settling time to ±0.05% overshoot slew rate	2V step 5V step 2V step 2V step	4.7 5.5 12 0 1200	<5.8 <6.5 <18 <5 >800	<5.8 <6.5 <18 <5 >800	<7.8 <8.0 <24 <5 >700	ns ns ns % V/μs	TRS TRL TSP OS SR
DISTORTION AND NOISE PER 2nd harmonic distortion 3rd harmonic distortion equivalent input noise ²	RFORMANCE 2V _{pp} , 20MHz 2V _{pp} , 20MHz	-45 -60	<-30 <-45	<-33 <-50	<-30 <-50	dBc dBc	HD2 HD3
noise floor integrated noise	>1MHz 1MHz to 100MHz	-158 28	<-156 <35	<-156 <35	<-155 <40	dBm(1Hz) μV	SNF INV
CLAMP PERFORMANCE overshoot in clamp overload recovery from clamp V _{io} drift after recovery * clamp accuracy input bias current on V _H , V _L - 3dB bandwidth useful clamping range	32x overdrive 32x overdrive >2x overdrive V _L , V _H = 2Vpp V _H or V _L	5 1 150 0.1 20 50	 <3 <200 <0.2 <100 <±3.0	<15 <3 <200 <0.2 <50 — <±3.3	 <3 <200 <0.2 <50 <±3.3	% ns μV V μA MHz	OVC TSO CDR VOC ICL CBW CMC
*static, DC PERFORMANCE *input offset voltage average temperature coefficien *input bias current average temperature coefficien *input bias current average temperature coefficien power supply rejection ratio common mode rejection ratio *supply current	non-inverting nt inverting	1.5 10 10 100 100 100 70 70 18	<4.6 <20 <37 <150 <46 <200 >55 >55 <25	<3.0 <25 - <30 - >60 >60 <24	<5.0 <20 <35 <100 <40 <100 >60 >60 <24	mV μV/°C μA nA/°C μA nA/°C dB dB mA	VIO DVIO IBN DIBN IBI DIBI PSRR CMRR ICC
miscellaneous perform non-inverting input output impedance common mode input range output voltage range output current	resistance capacitance at DC no load -40°C to +85°C -55°C to +125°C	150 4 0.2 3.0 ±3.5V ±60 ±60	>50 <7 <0.3 >2.0 >±3.0 >±35 >±30	>100 <7 <0.3 >2.5 >±3.2 >±50 >±50	>100 <7 <0.3 >2.5 >±3.2 >±50 >±50	$\begin{array}{c} k\Omega\\ pF\\ \Omega\\ V\\ V\\ mA\\ mA \end{array}$	RIN CIN RO CMIR VO IO

Min/max ratings are based on product characterization and simulation. Individual parameters are tested as noted. Outgoing quality levels are determined from tested parameters.

Absolute Maximum Ratings Miscellaneous Ratings V_{cc} ±7V recommended gain range: + 7 to + 50, - 1 to - 50 output is short circuit protected to lout ground, but maximum reliability will be NOTES: maintained if I_{out} does not exceed... common mode input voltage 100% tested at + 25°C, sample at + 85°C. 60mA ±V_{cc} + 150°C junction temperature Package Thermal Resistance operating temperature range -40°C to +85°C AJ: Package storage temperature range -65°C to + 150°C AJP 70°C/W 125°C/W lead solder duration (+ 300°C) 10 sec AJE 65°C/W 145°C/W ESD rating (human body model) <1000V **CERDIP** 45°C/W 135°C/W

Typical Performance Characteristics ($T_A = 25^\circ$, $A_V = +32$, $V_{CC} = \pm 5V$, $R_L = 100\Omega$, $R_f = 1.5\Omega$, $V_H = +3V$, $V_L = -3V$)



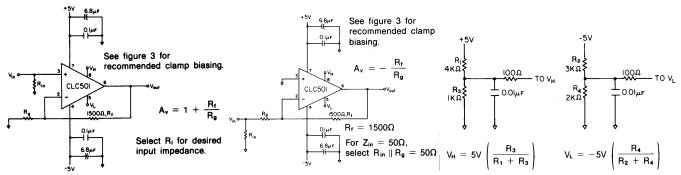


Figure 1: recommended non-inverting gain circuit

Figure 2: recommended inverting gain circuit

Figure 3: recommended clamp biasing for clamp levels of + 1V and -2V

Clamp Operation

The maximum positive or negative excursion of the output voltage is determined by voltages applied to the clamping pins, $V_{\rm H}$ and $V_{\rm L}$ $V_{\rm H}$ determines the positive clamping level; $V_{\rm L}$ determines the negative level. For example, if $V_{\rm H}$ is set at +2V and $V_{\rm L}$ is set at -0.5V the output voltage is restricted within this -0.5V to +2V range. When the output voltage tries to exceed this level, the amplifier goes into "clamp mode" and the output voltage limits at the clamp voltage.

Clamp Accuracy and Amplifier Linearity

Ideally, the clamped output voltage and the clamp voltage should be identical. In practice, however, there are two sources of clamp inaccuracy: the inherent clamp accuracy (which is shown in the specification page) and resistor divider action of open-loop output resistance of 10Ω and the load resistor. Or, in equation form,

$$V_{\text{out, clamp}} \,=\, (V_{\text{H or L}} \,\pm 200 \text{mV}) \,\, \frac{R_{\text{L}}}{R_{\text{L}} \,+\, 10\Omega.} \label{eq:Vout, clamp}$$

When setting the clamp voltages, the designer should also recognize that within about 200mV of the clamp voltage, amplifier linearity begins to deteriorate. (See plot on previous page.)

Biasing V_H and V_L

Each of the clamping pins is buffered internally so simple resistive voltage divider circuits work well in providing the clamp voltages (see Figure 3). The 100Ω isolating resistor ensures stability when the clamp pin is connected to V_{cc} or when the clamp pin is driven by an external signal source; in other situations, such as the one described in Figure 3, the isolating resistor is not necessary.

 V_H should be biased more positively than V_L . V_H may be biased below 0V; however, with this biasing, the output voltage will actually clamp at 0V unless a simple pull down circuit is added to the op amp output. (When clamped against V_H , the output cannot sink current.) An analogous situation and design solution exists for V_L when it is biased above 0V, but in this case, a pull up circuit is used to *source* current when the amplifier is clamped against V_L .

The clamps, which have a bandwidth of about 50MHz, may be driven by a high-frequency signal source. This allows the clamping level to be modulated, which is useful in many applications such as pulse amplitude modulation. The source resistance of the signal source should be less than 500Ω to ensure stability.

Clamp-Mode Dynamics

As can be seen in the clamped pulse response plot on the previous page, clamping is virtually instantaneous. Note, however, that there can be a small amount of overshoot, as indicated on the specification page. The output voltage stays at the clamp voltage level as long as the product of the input voltage and the gain setting exceeds the clamp voltage. When the input voltage decreases, it will eventually reach a point where it is no longer trying to drive the output voltage above the clamp voltage. When this occurs, there is typically a 1ns "overload recovery from clamp," which is the time it takes for the op amp to resume linear operation. The normal op amp parameters, such as the rise time, apply when the op amp is in linear operation.

When the op amp is in clamp mode for more than about 100ns, a small thermal tail can be detected in the settling performance. This tail, which has a maximum value of $200\mu V$ referred to the input, is proportional to the amount of time spent in clamp mode. In most

applications, this will have only a minor effect. For example, in a system with a 100ns overdrive occurring with a duty cycle of 10%, the input-referred tail is $20\mu V$ which is only 0.001% of a 2V signal.

DC Accuracy and Noise

Since the two inputs for the CLC501 are quite dissimilar, the noise and offset error performance differs somewhat from that of a standard differential input amplifier. Specifically, the inverting input current noise is much larger than the non-inverting current noise. Also the two input bias currents are physically unrelated rendering bias current cancellation through matching of the inverting and non-inverting pin resistors ineffective.

In Equation 3, the output offset is the algebraic sum of the equivalent input voltage and current sources that influence DC operation. Output noise is determined similarly except that a root-sum-of-squares replaces the algebraic sum. $R_{\text{\tiny 8}}$ is the non-inverting pin resistance.

Output Offset
$$V_o = \pm IBN \times R_s (1 + R_t/R_g) \pm VIO (1 + R_t/R_g) \pm IBI \times R_t$$
 Eq. (3)

PSRR and CMRR

The PSRR and CMRR performance plots on the previous page show performance for a circuit set at a gain of ± 32 and a source resistance of $0\Omega.$ In current feedback op amps, common mode and power supply variations manifest themselves in changes in the op amp's bias currents (IBI for the inverting input and IBN for the non-inverting input) and in the offset voltage (VIO). At DC, these values are:

CMRR:
$$\frac{\Delta \text{VIO}}{\Delta \text{V}_{cm}} = 130 \mu \text{V/V}$$
 PSRR: $\frac{\Delta \text{VIO}}{\Delta \text{V}_{cc}} = 180 \mu \text{V/V}$ $\frac{\Delta \text{IBN}}{\Delta \text{V}_{cm}} = 6 \mu \text{A/V}$ $\frac{\Delta \text{IBI}}{\Delta \text{V}_{cm}} = 2 \mu \text{A/V}$ $\frac{\Delta \text{IBI}}{\Delta \text{V}_{cc}} = 3 \mu \text{A/V}$

The total effect, as referenced to the input, is given by the following:

$$\begin{split} \text{PSRR:} &= -20 \text{ log } \left[\frac{\Delta \text{VIO}}{\Delta \text{V}_{\text{cc}}} + \frac{\Delta \text{IBN}}{\Delta \text{V}_{\text{cc}}} \; \text{R}_{\text{s}} + \frac{\Delta \text{IBI}}{\Delta \text{V}_{\text{cc}}} \; \text{R}_{\text{eq}} \right] \\ \text{CMRR} &= -20 \text{ log } \left[\frac{\Delta \text{VIO}}{\Delta \text{V}_{\text{cm}}} + \frac{\Delta \text{IBN}}{\Delta \text{V}_{\text{cm}}} \; \text{R}_{\text{s}} + \frac{\Delta \text{IBI}}{\Delta \text{V}_{\text{cm}}} \; \text{R}_{\text{eq}} \right] \end{split}$$

Where R_s is the equivalent resistance seen by the non-inverting input and R_{eq} is the equivalent resistance of R_g in parallel with R_f .

Printed Circuit Layout

As with any high frequency device, a good PCB layout will enhance performance. Ground plane construction and good power supply bypassing close to the package are critical to achieving full performance. In the non-inverting configuration, the amplifier is sensitive to stray capacitance to ground at the inverting input. Hence, the inverting node connections should be small with minimal coupling to the ground plane. Shunt capacitance across the feedback resistor should not be used to compensate for this

Evaluation PC boards (part number CLC730013 for through-hole and CLC730027 for SOIC) for the CLC501 are avalible.

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6