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# **Ordering Information**

Package	Temperatu	re Range	NSC	Transport Media	
	Military	Industrial	Drawing		
14-Pin	LPC660AMD		D14E	Rail	
Side Brazed					
Ceramic DIP					
14-Pin		LPC660AIM	M14A	Rail	
Small Outline		or LPC660IM		Tape and Reel	
14-Pin		LPC660AIN	N14A	Rail	
Molded DIP		or LPC660IN			
14-Pin	LPC660AMJ/883		J14A	Rail	
Ceramic DIP					

### Absolute Maximum Ratings (Note 3)

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If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

### **Operating Ratings** (Note 3)

Differential Input Voltage Supply Voltage (V <sup>+</sup> - V <sup>-</sup> )	±Supply Voltage 16V
Output Short Circuit to V <sup>+</sup>	(Note 11)
Output Short Circuit to V <sup>-</sup>	(Note 1)
Lead Temperature	
(Soldering, 10 sec.)	260°C
Storage Temp. Range	-65°C to +150°C
Junction Temperature (Note 2)	150°C
ESD Rating	
(C = 100 pF, R = 1.5 kΩ)	1000V
Power Dissipation	(Note 2)
Current at Input Pin	±5 mA
Current at Output Pin	±18 mA

Temperature Range	
LPC660AM	$-55^{\circ}C \le T_{J} \le +125^{\circ}C$
LPC660AI	$-40^{\circ}C \le T_{J} \le +85^{\circ}C$
LPC660I	$-40^{\circ}C \le T_{J} \le +85^{\circ}C$
Supply Range	4.75V to 15.5V
Power Dissipation	(Note 9)
Thermal Resistance ( $\theta_{JA}$ ), (Note 10)	
14-Pin Ceramic DIP	90°C/W
14-Pin Molded DIP	85°C/W
14-Pin SO	115°C/W
14-Pin Side Brazed Ceramic DIP	90°C/W

### **DC Electrical Characteristics**

Unless otherwise specified, all limits guaranteed for $T_{J} = 25^{\circ}C$ . Boldface limits apply at the temperature extremes. V <sup>+</sup> = 5V, V <sup>-</sup>	-
= 0V, $V_{CM}$ = 1.5V, $V_O$ = 2.5V, and $\overline{R_L}$ > 1M unless otherwise specified.	

Parameter	Conditions	Тур	LPC660AM LPC660AMJ/883	LPC660AI	LPC660I	Units
			Limit	Limit	Limit	
			(Notes 4, 8)	(Note 4)	(Note 4)	
Input Offset Voltage		1	3	3	6	mV
			3.5	3.3	6.3	max
Input Offset Voltage		1.3				µV/°C
Average Drift						
Input Bias Current		0.002	20			pА
			100	4	4	max
Input Offset Current		0.001	20			pА
			100	2	2	max
Input Resistance		>1				Tera Ω
Common Mode	$0V \le V_{CM} \le 12.0V$	83	70	70	63	dB
Rejection Ratio	V <sup>+</sup> = 15V		68	68	61	min
Positive Power Supply	$5V \le V^+ \le 15V$	83	70	70	63	dB
Rejection Ratio			68	68	61	min
Negative Power Supply	$0V \le V^- \le -10V$	94	84	84	74	dB
Rejection Ratio			82	83	73	min
Input Common Mode	V <sup>+</sup> = 5V & 15V	-0.4	-0.1	-0.1	-0.1	V
Voltage Range	For CMRR > 50 dB		0	0	0	max
		V <sup>+</sup> – 1.9	V <sup>+</sup> – 2.3	V <sup>+</sup> – 2.3	V <sup>+</sup> – 2.3	V
			V <sup>+</sup> – 2.6	V+ – 2.5	V <sup>+</sup> – 2.5	min
Large Signal	$R_L$ = 100 k $\Omega$ (Note 5)	1000	400	400	300	V/mV
Voltage Gain	Sourcing		250	300	200	min
	Sinking	500	180	180	90	V/mV
			70	120	70	min
	$R_L = 5 k\Omega$ (Note 5)	1000	200	200	100	V/mV
	Sourcing		150	160	80	min
	Sinking	250	100	100	50	V/mV
			35	60	40	min

Parameter	Conditions	Тур	LPC660AM LPC660AMJ/883	LPC660AI	LPC660I Limit	= 5V, V <sup>_</sup> Units
			Limit	Limit		
			(Notes 4, 8)	(Note 4)	(Note 4)	
Output Swing	V <sup>+</sup> = 5V	4.987	4.970	4.970	4.940	v
ouput owing	$R_1 = 100 \text{ k}\Omega \text{ to V}^+/2$	1.007	4.950	4.950	4.910	min
		0.004	0.030	0.030	0.060	V
			0.050	0.050	0.090	max
	V <sup>+</sup> = 5V	4.940	4.850	4.850	4.750	V
	$R_1 = 5 k\Omega$ to V <sup>+</sup> /2		4.750	4.750	4.650	min
		0.040	0.150	0.150	0.250	V
			0.250	0.250	0.350	max
	V <sup>+</sup> = 15V	14.970	14.920	14.920	14.880	V
	$R_L = 100 \text{ k}\Omega \text{ to V}^+/2$		14.880	14.880	14.820	min
		0.007	0.030	0.030	0.060	V
			0.050	0.050	0.090	max
	V <sup>+</sup> = 15V	14.840	14.680	14.680	14.580	V
	$R_L = 5 k\Omega$ to V <sup>+</sup> /2		14.600	14.600	14.480	min
		0.110	0.220	0.220	0.320	V
			0.300	0.300	0.400	max
Dutput Current	Sourcing, $V_O = 0V$	22	16	16	13	mA
V <sup>+</sup> = 5V			12	14	11	min
	Sinking, $V_{O} = 5V$	21	16	16	13	mA
			12	14	11	min
Dutput Current	Sourcing, $V_O = 0V$	40	19	28	23	mA
/+ = 15V			19	25	20	min
	Sinking, $V_{O} = 13V$	39	19	28	23	mA
	(Note 11)		19	24	19	min
Supply Current	All Four Amplifiers	160	200	200	240	μA
	V <sub>O</sub> = 1.5V		250	230	270	max

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Unless otherwise specified, all limits guaranteed for  $T_J$  = 25°C. **Boldface** limits apply at the temperature extremes. V<sup>+</sup> = 5V, V<sup>-</sup> = 0V, V<sub>CM</sub> = 1.5V, V<sub>O</sub> = 2.5, and R<sub>L</sub> > 1M unless otherwise specified.

Parameter	Conditions	Тур	LPC660AM	LPC660AI	LPC660I	Units
			LPC660AMJ/883			
			Limit	Limit	Limit	1
			(Notes 4, 8)	(Note 4)	(Note 4)	
Slew Rate	(Note 6)	0.11	0.07	0.07	0.05	V/µs
			0.04	0.05	0.03	min
Gain-Bandwidth Product		0.35				MHz
Phase Margin		50				Deg
Gain Margin		17				dB
Amp-to-Amp Isolation	(Note 7)	130				dB
Input Referred Voltage Noise	F = 1 kHz	42				nV/√Hz
Input Referred Current Noise	F = 1 kHz	0.0002				pA/√Hz
Total Harmonic Distortion	$F = 1 \text{ kHz}, A_V = -10$	0.01				%
	$R_L$ = 100 k $\Omega$ , $V_O$ = 8 $V_{PP}$					

Note 1: Applies to both single supply and split supply operation. Continuous short circuit operation at elevated ambient temperature and/or multiple Op Amp shorts can result in exceeding the maximum allowed junction temperature of 150°C. Output currents in excess of  $\pm 30$  mA over long term may adversely affect reliability. Note 2: The maximum power dissipation is a function of  $T_{J(max)}$ ,  $\theta_{JA}$  and  $T_A$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(max)}^{-1} - T_A)\theta_{JA}$ .

Note 3: Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but do not guarantee specific performance limits. For guaranteed specifications and test conditions, see the Electrical Characteristics. The guaranteed specifications apply only for the test conditions listed.

Note 4: Limits are guaranteed by testing or correlation.

Note 5: V<sup>+</sup> = 15V, V<sub>CM</sub> = 7.5V and R<sub>L</sub> connected to 7.5V. For Sourcing tests, 7.5V  $\leq$  V<sub>O</sub>  $\leq$  11.5V. For Sinking tests, 2.5V  $\leq$  V<sub>O</sub>  $\leq$  7.5V.

Note 6: V<sup>+</sup> = 15V. Connected as Voltage Follower with 10V step input. Number specified is the slower of the positive and negative slew rates.

Note 7: Input referred. V<sup>+</sup> = 15V and R<sub>L</sub> = 100 k $\Omega$  connected to V<sup>+</sup>/2. Each amp excited in turn with 1 kHz to produce V<sub>O</sub> = 13 V<sub>PP</sub>.

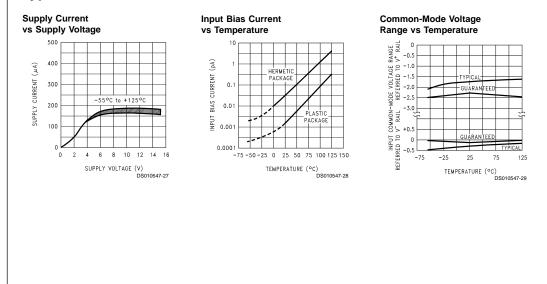
Note 8: A military RETS electrical test specification is available on request. At the time of printing, the LPC660AMJ/883 RETS specification complied fully with the boldface limits in this column. The LPC660AMJ/883 may also be procured to a Standard Military Drawing specification.

Note 9: For operating at elevated temperatures, the device must be derated based on the thermal resistance  $\theta_{JA}$  with  $P_D = (T_J - T_A)/\theta_{JA}$ .

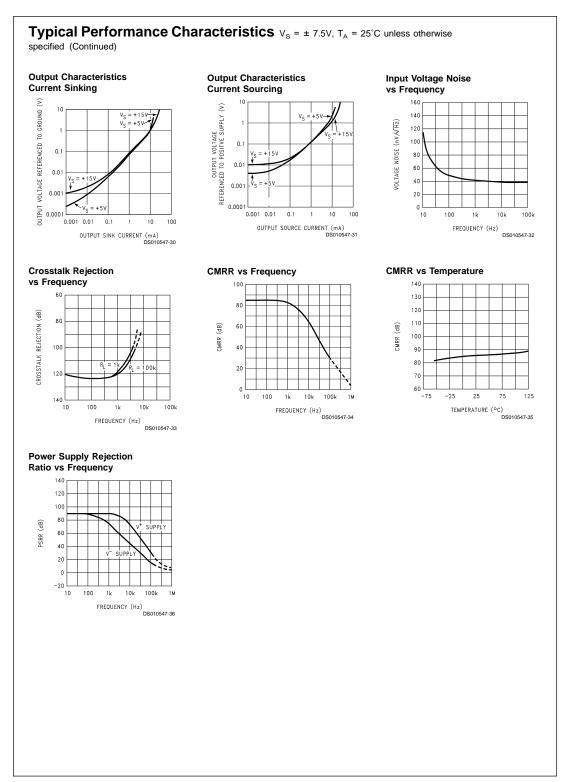
Note 10: All numbers apply for packages soldered directly into a PC board.

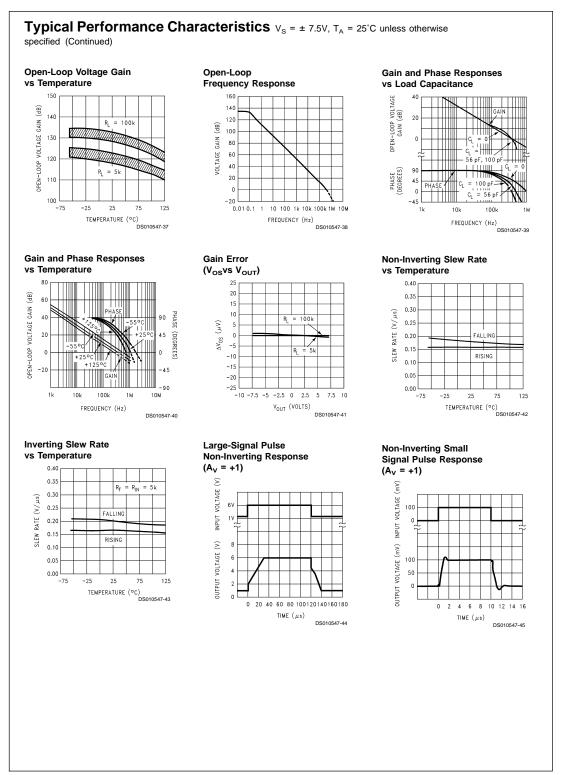
Note 11: Do not connect output to V<sup>+</sup>when V<sup>+</sup> is greater than 13V or reliability may be adversely affected.

#### Typical Performance Characteristics $V_s = \pm 7.5V$ , $T_A = 25^{\circ}C$ unless otherwise specified

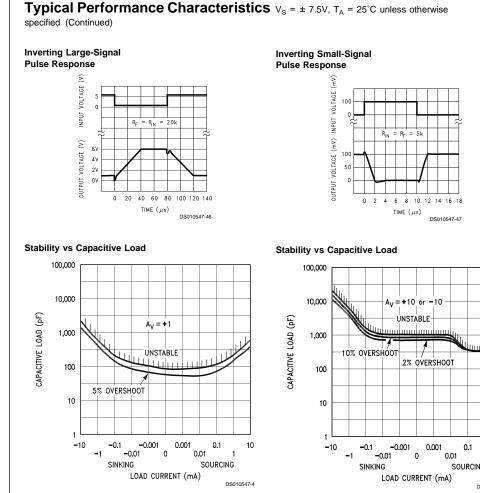


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Note: Avoid resistive loads of less than  $500\Omega$ , as they may cause instability.

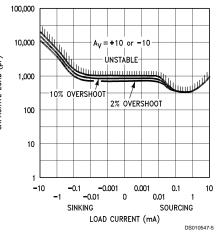
### **Application Hints**

### AMPLIFIER TOPOLOGY

The topology chosen for the LPC660 is unconventional (compared to general-purpose op amps) in that the traditional unity-gain buffer output stage is not used; instead, the output is taken directly from the output of the integrator, to allow rail-to-rail output swing. Since the buffer traditionally delivers the power to the load, while maintaining high op amp gain and stability, and must withstand shorts to either rail, these tasks now fall to the integrator.

As a result of these demands, the integrator is a compound affair with an embedded gain stage that is doubly fed forward (via  $C_f$  and  $C_{ff}$ ) by a dedicated unity-gain compensation driver. In addition, the output portion of the integrator is a push-pull configuration for delivering heavy loads. While sinking current the whole amplifier path consists of three gain stages with one stage fed forward, whereas while sourcing the path contains four gain stages with two fed forward.

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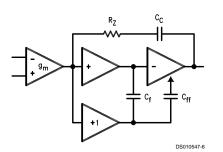


FIGURE 1. LPC660 Circuit Topology (Each Amplifier)

The large signal voltage gain while sourcing is comparable to traditional bipolar op amps, for load resistance of at least 5 k $\Omega.$  The gain while sinking is higher than most CMOS op

#### Application Hints (Continued)

amps, due to the additional gain stage; however, when driving load resistance of 5 k $\Omega$  or less, the gain will be reduced as indicated in the Electrical Characteristics. The op amp can drive load resistance as low as 500 $\Omega$  without instability.

#### COMPENSATING INPUT CAPACITANCE

Refer to the LMC660 or LMC662 datasheets to determine whether or not a feedback capacitor will be necessary for compensation and what the value of that capacitor would be.

#### CAPACITIVE LOAD TOLERANCE

Like many other op amps, the LPC660 may oscillate when its applied load appears capacitive. The threshold of oscillation varies both with load and circuit gain. The configuration most sensitive to oscillation is a unity-gain follower. See the Typical Performance Characteristics.

The load capacitance interacts with the op amp's output resistance to create an additional pole. If this pole frequency is sufficiently low, it will degrade the op amp's phase margin so that the amplifier is no longer stable at low gains. The addition of a small resistor ( $50\Omega$  to  $100\Omega$ ) in series with the op amp's output, and a capacitor (5 pF to 10 pF) from inverting input to output pins, returns the phase margin to a safe value without interfering with lower-frequency circuit operation. Thus, larger values of capacitance can be tolerated without oscillation. Note that in all cases, the output will ring heavily when the load capacitance is near the threshold for oscillation.

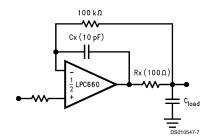


FIGURE 2. Rx, Cx Improve Capacitive Load Tolerance

Capacitive load driving capability is enhanced by using a pull up resistor to V<sup>+</sup> (*Figure 3*). Typically a pull up resistor conducting 50  $\mu$ A or more will significantly improve capacitive load responses. The value of the pull up resistor must be determined based on the current sinking capability of the ampli-

fier with respect to the desired output swing. Open loop gain of the amplifier can also be affected by the pull up resistor (see Electrical Characteristics).

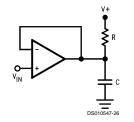
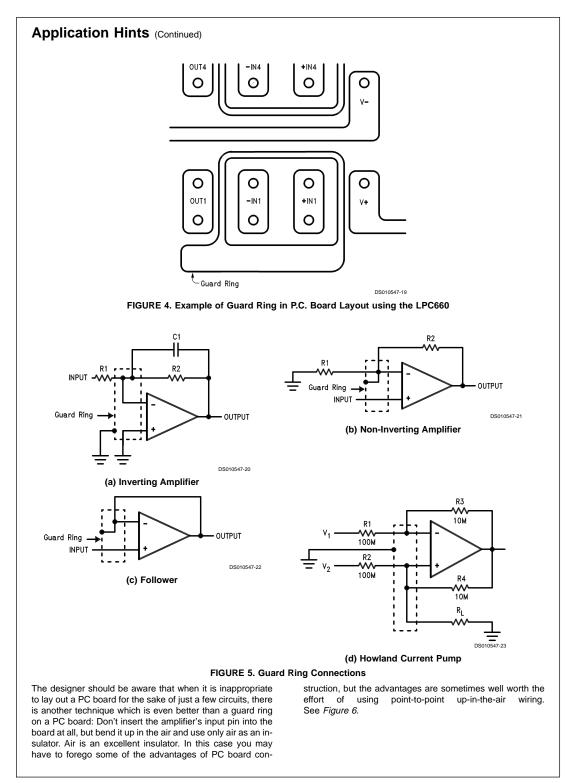


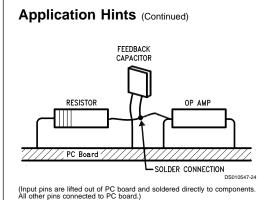
FIGURE 3. Compensating for Large Capacitive Loads with A Pull Up Resistor

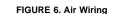
#### PRINTED-CIRCUIT-BOARD LAYOUT FOR HIGH-IMPEDANCE WORK

It is generally recognized that any circuit which must operate with less than 1000 pA of leakage current requires special layout of the PC board. When one wishes to take advantage of the ultra-low bias current of the LPC660, typically less than 0.04 pA, it is essential to have an excellent layout. Fortunately, the techniques for obtaining low leakages are quite simple. First, the user must not ignore the surface leakage of the PC board, even though it may sometimes appear acceptably low, because under conditions of high humidity or dust or contamination, the surface leakage will be appreciable.

To minimize the effect of any surface leakage, lay out a ring of foil completely surrounding the LPC660's inputs and the terminals of capacitors, diodes, conductors, resistors, relay terminals, etc. connected to the op-amp's inputs. See Figure 4. To have a significant effect, guard rings should be placed on both the top and bottom of the PC board. This PC foil must then be connected to a voltage which is at the same voltage as the amplifier inputs, since no leakage current can flow between two points at the same potential. For example, a PC board trace-to-pad resistance of 1012 ohms, which is normally considered a very large resistance, could leak 5 pA if the trace were a 5V bus adjacent to the pad of an input. This would cause a 100 times degradation from the LPC660's actual performance. However, if a guard ring is held within 5 mV of the inputs, then even a resistance of 10<sup>11</sup> ohms would cause only 0.05 pA of leakage current, or perhaps a minor (2:1) degradation of the amplifier's performance. See Figure 5a, Figure 5b, Figure 5c for typical connections of guard rings for standard op-amp configurations. If both inputs are active and at high impedance, the guard can be tied to ground and still provide some protection; see Figure 5d.







#### BIAS CURRENT TESTING

The test method of *Figure 7* is appropriate for bench-testing bias current with reasonable accuracy. To understand its operation, first close switch S2 momentarily. When S2 is opened, then

$$I^- = \frac{dV_{OUT}}{dt} \times C2.$$

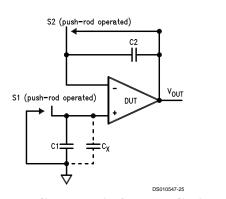


FIGURE 7. Simple Input Bias Current Test Circuit

A suitable capacitor for C2 would be a 5 pF or 10 pF silver mica, NPO ceramic, or air-dielectric. When determining the magnitude of  $I^-$ , the leakage of the capacitor and socket must be taken into account. Switch S2 should be left shorted most of the time, or else the dielectric absorption of the capacitor C2 could cause errors.

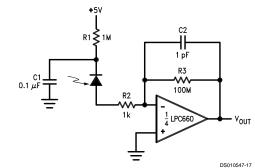
Similarly, if S1 is shorted momentarily (while leaving S2 shorted)

$$I^{+} = \frac{dV_{OUT}}{dt} \times (C1 + C_{x})$$

where  $C_x$  is the stray capacitance at the + input.

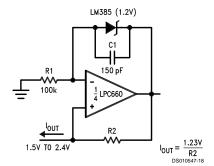
## Typical Single-Supply Applications $(V^+ = 5.0 V_{DC})$

Photodiode Current-to-Voltage Converter



Note: A 5V bias on the photodiode can cut its capacitance by a factor of 2 or 3, leading to improved response and lower noise. However, this bias on the photodiode will cause photodiode leakage (also known as its dark current).

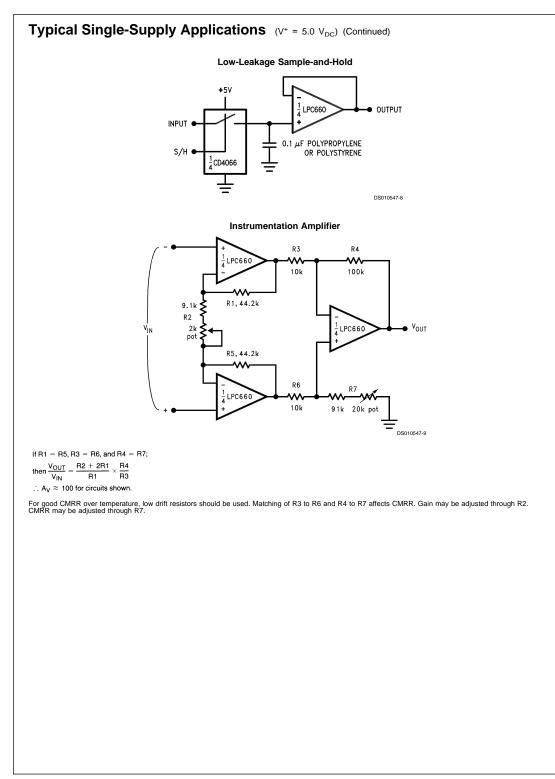
**Micropower Current Source** 



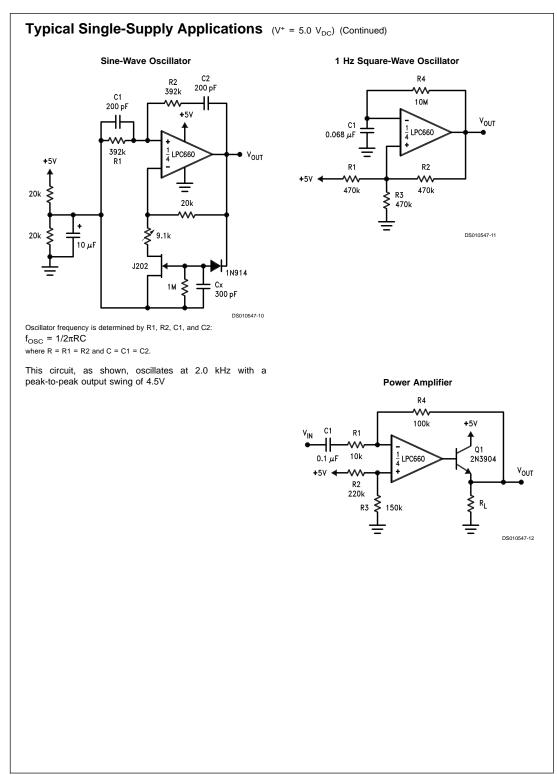
Note: (Upper limit of output range dictated by input common-mode range; lower limit dictated by minimum current requirement of LM385.)

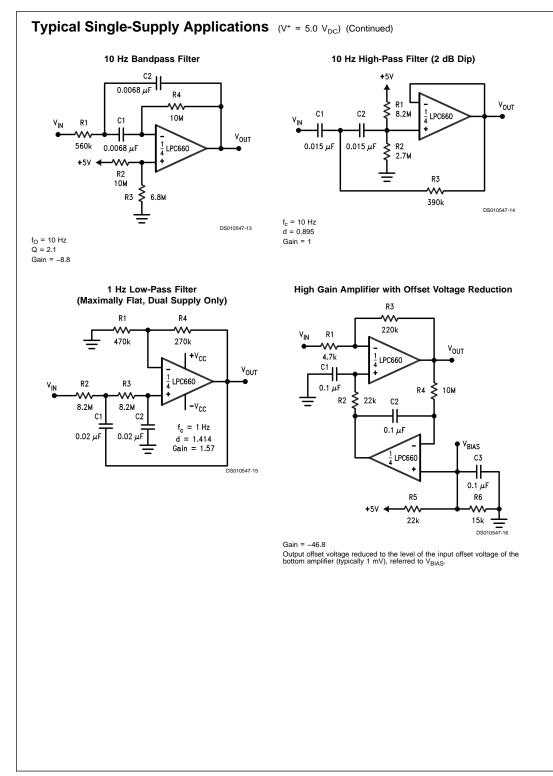
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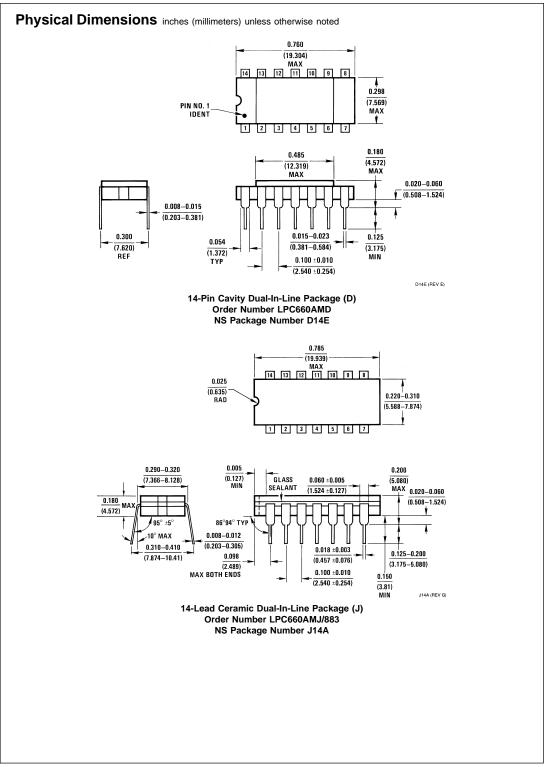
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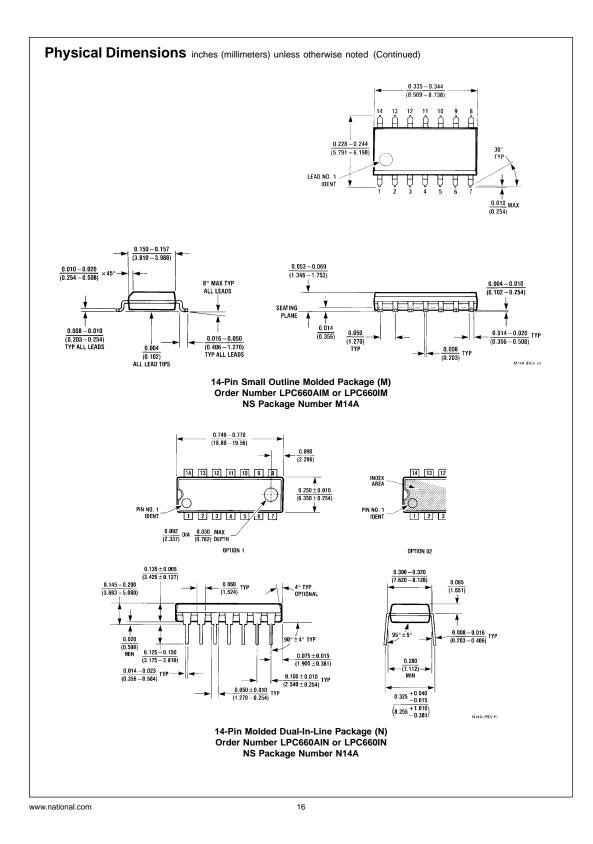


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