## DATA SHEET

## UMA1022M Low cost dual frequency synthesizer for radio telephones

Product specification
Supersedes data of 1998 May 15
File under Integrated Circuits, IC17

Low cost dual frequency synthesizer for radio telephones

## FEATURES

- Low phase noise
- Low current from 3 V supply
- Fully programmable dividers
- 3-line serial interface bus
- Input reference buffer configurable as an oscillator with external crystal resonator
- Wide compliance voltage charge pump outputs
- Two power-down input control pins.


## APPLICATIONS

- 900 MHz and 2 GHz digital radio telephones
- Portable battery-powered radio equipment.


## GENERAL DESCRIPTION

The UMA1022M BICMOS device integrates prescalers, programmable dividers, a crystal oscillator/buffer and phase comparators to implement two phase-locked loops. The device is designed to operate from 3 NiCd or a single Lilon cell in pocket phones, or from an external 3 V supply.

The synthesizers operate at RF input frequencies up to 2.1 GHz and 550 MHz . All divider ratios are supplied via a 3 -wire serial programming bus. The reference divider uses a common, fully programmable part and a separate subdivider section. In this way the comparison frequencies are related to each other allowing optimum isolation between charge pump pulses.

Separate power and ground pins are provided to the analog (charge pump, prescaler) and digital (CMOS) circuits. An independent supply for the crystal oscillator section allows maximum frequency stability. The ground leads should be externally short-circuited to prevent large currents flowing across the die and thus causing damage. $\mathrm{V}_{\mathrm{DD}}$ and $\mathrm{V}_{\mathrm{DD}}$ must be at the same potential. $\mathrm{V}_{\mathrm{CCA}}$ and $V_{\text {CCB }}$ must be equal to each other and equal to or greater than $\mathrm{V}_{\mathrm{DD}}$ (e.g. $\mathrm{V}_{\mathrm{DD}}=3 \mathrm{~V}$ and $\mathrm{V}_{\mathrm{CCA}}=5.5 \mathrm{~V}$ for wider VCO control voltage range).

The charge pump currents (phase detector gain) are fixed by internal resistances and controlled by the serial interface. Only passive loop filters are necessary; the charge pumps function within a wide voltage compliance range to improve the overall system performance.

Suitable pin layout is chosen to minimize coupling and interference between signals entering or leaving the chip.

## QUICK REFERENCE DATA

| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $V_{\text {DD }}$ | digital supply voltage | $\mathrm{V}_{\text {CCA }}=\mathrm{V}_{\text {CCB }} \geq \mathrm{V}_{\text {DD }}$ | 2.7 | 3.0 | 5.5 | V |
| $\mathrm{V}_{\text {CCA }}, \mathrm{V}_{\text {CCB }}$ | analog supply voltages | $\mathrm{V}_{\text {CCA }}=\mathrm{V}_{\text {CCB }} \geq \mathrm{V}_{\text {DD }}$ | 2.7 | 3.0 | 5.5 | V |
| $\mathrm{V}_{\text {DDX }}$ | crystal reference supply voltage | $\mathrm{V}_{\mathrm{DDX}}=\mathrm{V}_{\mathrm{DD}}$ | 2.7 | 3.0 | 5.5 | V |
| $I_{\text {tot }}$ | all supply currents $\left(I_{D D}+I_{C C A}+I_{C C B}+I_{D D X}\right)$ in active mode | $\begin{aligned} & \overline{\mathrm{E}}=1 ; \mathrm{V}_{\mathrm{CCA}}=\mathrm{V}_{\mathrm{CCB}}=3.0 \mathrm{~V} ; \\ & \mathrm{V}_{\mathrm{DDX}}=\mathrm{V}_{\mathrm{DD}}=3.0 \mathrm{~V} \\ & \mathrm{XON}=0 \\ & \mathrm{XON}=1 \end{aligned}$ | - | $\begin{aligned} & 14.65 \\ & 15.9 \end{aligned}$ |  | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| $I_{\text {tot(pd) }}$ | total supply currents in power-down mode |  | - | 40 | - | $\mu \mathrm{A}$ |
| $\mathrm{f}_{\mathrm{RF}}$ | RF input frequency |  | 300 | - | 2100 | MHz |
| $\mathrm{f}_{\mathrm{IF}}$ | IF input frequency | $\mathrm{V}_{\text {CCA }}=\mathrm{V}_{\text {CCB }} \leq 4.0 \mathrm{~V}$ | 50 | - | 550 | MHz |
|  |  |  | 50 | - | 400 | MHz |
| $\mathrm{f}_{\text {xtal }}$ | crystal reference oscillator frequency |  | 3 | - | 20 | MHz |
| $\mathrm{f}_{\mathrm{PCmax}}$ | maximum loop comparison frequency |  | - | 2000 | - | kHz |
| $\mathrm{T}_{\text {amb }}$ | operating ambient temperature |  | -30 | - | +85 | ${ }^{\circ} \mathrm{C}$ |

## Low cost dual frequency synthesizer for

## radio telephones

ORDERING INFORMATION

| TYPE NUMBER | PACKAGE |  |  |
| :--- | :---: | :---: | :---: |
|  | NAME | DESCRIPTION | VERSION |
| UMA1022M | SSOP20 | plastic shrink small outline package; 20 leads; body width 4.4 mm | SOT266-1 |

## BLOCK DIAGRAM



Fig. 1 Block diagram.

## Low cost dual frequency synthesizer for radio telephones

PINNING

| SYMBOL | PIN | DESCRIPTION |
| :--- | :---: | :--- |
| $\overline{\text { XIN }}$ | 1 | inverting crystal reference input |
| XGND | 2 | ground for crystal oscillator circuits |
| XOUT | 3 | crystal oscillator buffer output |
| CP $_{\mathrm{B}}$ | 4 | IF synthesizer charge pump output |
| $\mathrm{V}_{\mathrm{CCB}}$ | 5 | analog supply to IF synthesizer |
| $\mathrm{IF}_{\mathrm{B}}$ | 6 | IF VCO main divider input |
| ON $_{\mathrm{B}}$ | 7 | $\begin{array}{l}\text { IF power-on input; ON } \\ \text { B }\end{array}$ |
| means HIGH |  |  |
| means synthesizer is active |  |  |$]$



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## FUNCTIONAL DESCRIPTION

## Main dividers

The main dividers are clocked at pin $\mathrm{RF}_{\mathrm{A}}$ by the RF oscillator signal and at pin $\mathrm{IF}_{\mathrm{B}}$ by the IF oscillator signal. The inputs are AC coupled through external capacitors. Input impedances are high, dominated by parasitic package capacitances, so matching is off-chip. The sensitive dividers operate with signal levels from 35 to 225 mV (RMS), at frequencies up to 2.1 GHz (RF part) and up to 550 MHz (IF part). Both include programmable bipolar prescalers followed by CMOS counters. The RF main divider allows programmable ratios from 512 to 65535; the IF blocks accept values between 128 and 16383.

## Crystal oscillator

A fully differential low-noise amplifier/buffer is integrated providing outputs to drive other circuits, and to build a crystal oscillator; only needed are an external resonance circuit and tuning elements (temperature compensation). A bus controlled power-down mode disables the low-noise amplifier to reduce current if not needed.

The normal differential input pins drive a clock buffer to provide edges to the programmable reference divider at frequencies up to 20 MHz . The inputs are AC coupled through external capacitors, and operate with signals down to 35 mV (RMS) and up to 0.5 V (RMS).

Various crystal oscillator structures can be built using the amplifier. By coupling one output back to the appropriate input through the resonator, and decoupling the other input to ground, the second output becomes available to deliver the reference frequency to other circuits.

## Reference dividers

A first common divider circuit produces an output frequency for RF or IF synthesizer phase comparison, depending on the P/A bit. It drives a second independent divider, which delivers the reference edge to the IF or RF synthesizer phase comparator. When P/A is logic 1 , the output of the subdivider is connected to the RF phase comparator, whereas the output of the common divider is connected to the IF phase detector.

The phase comparators run at related frequencies with a controlled phase difference to avoid interference when in-lock. The common 10-bit section permits divide ratios from 8 to 1023; the second subdivider allows phase comparison frequency ratios between 1 and 16. Table 2 indicates how to program the corresponding bits to get the wanted ratio.

## Phase comparators

The phase detectors are driven by the output edges selected by the main and reference dividers. Each generates lead and lag signals to control the appropriate charge pump. The pumps output current pulses appear at pins $\mathrm{CP}_{\mathrm{A}}$ (RF synthesizer) and $\mathrm{CP}_{\mathrm{B}}$ (IF synthesizer). The current pulse duration is at least equal to the difference in time of arrival of the edges from the two dividers. If the main divider edge arrives first, $\mathrm{CP}_{\mathrm{A}}$ or $\mathrm{CP}_{\mathrm{B}}$ sink current. If the reference divider edge arrives first, $\mathrm{CP}_{\mathrm{A}}$ or $\mathrm{CP}_{\mathrm{B}}$ source current. For correct PLL operation the VCOs need to have a positive frequency/voltage control slope.

The currents at $\mathrm{CP}_{\mathrm{A}}$ and $\mathrm{CP}_{\mathrm{B}}$ are programmed via the serial bus as multiples of an internally-set reference current. The passage into power-down mode is synchronized with respect to the phase detector to prevent output current pulses being interrupted. Additional circuitry is included to ensure that the gain of the phase comparators remains linear even for small phase errors.

## Serial programming bus

A simple 3-line unidirectional serial bus is used to program the circuit. The 3 lines are DATA, clock (CLK) and enable ( $\overline{\mathrm{E}}$ ). The data sent to the device is loaded in bursts framed by $\overline{\mathrm{E}}$. Programming clock edges and their appropriate data bits are ignored until $\bar{E}$ goes active LOW. The programmed information is loaded into the addressed latch when $\overline{\mathrm{E}}$ returns HIGH. During normal operation, $\overline{\mathrm{E}}$ should be kept HIGH. Only the last 19 bits serially clocked into the device are retained within the programming register.

Additional leading bits are ignored, and no check is made on the number of clock pulses. The NMOS-rich design uses virtually no current when the bus is inactive; power-up is initiated when enable is taken LOW, and power-down occurs a short time after enable returns HIGH. Bus activity is allowed when either synthesizer is active or in power-down ( $\mathrm{ON}_{\mathrm{A}}$ and $\mathrm{ON}_{\mathrm{B}}$ inputs LOW) mode. Fully static CMOS registers retain programmed data whatever the power-down state, as long as the supply voltage is present.

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## Data format

The leading bits (dt15 to dt0) make up the data field, while the trailing three bits (ad2 to ad0) comprise an address field. The UMA1022M uses 4 of the 8 available addresses. The data format is shown in Table 1. The first bit entered is dt 15 , the last bit is ad0. For the divider ratios, the first bits entered ( P 0 and R0) are the Least Significant Bits (LSB). This is different from previous Philips synthesizers.

The trailing address bits are decoded on the rising edge of $\overline{\mathrm{E}}$. This produces an internal load pulse to store the data in the addressed latch. To avoid erroneous divider ratios, the load pulse is not allowed during data reads by the frequency dividers. This condition is guaranteed by respecting a minimum $\bar{E}$ pulse width after data transfer. The test register bits should not normally be programmed active (HIGH); normal operation requires them set LOW. When the supply voltage is established an internal power-up initialization pulse is generated to preconfigure the circuit state. Production testing does not verify that all bits are preconfigured correctly.

## Power-down mode

The RF and IF synthesizers are on when respectively the input signal $\mathrm{ON}_{\mathrm{A}}$ and $\mathrm{ON}_{\mathrm{B}}$ are HIGH. When turned on, the dividers and phase detector are synchronized to avoid random phase errors. When turned off, the phase detector is synchronized to avoid interrupting charge pump pulses. The UMA1022M has a very low current consumption in the power-down mode.

Table 1 Bit allocation; note 1

| FIRS | T IN |  |  |  |  | REG | STE | R BIT | ALL | OCA | ION |  |  |  |  |  | LAS | T IN |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | DATA | FIEL |  |  |  |  |  |  |  |  |  | DRE |  |
| dt15 | dt14 | dt13 | dt12 | dt11 | dt10 | dt9 | dt8 | dt7 | dt6 | dt5 | dt4 | dt3 | dt2 | dt1 | dt0 | ad2 | ad1 | ado |
| Test bits ${ }^{(2)}$ |  |  |  | CPI | S/D | XON ${ }^{(3)}$ | X | X | X | X | $\mathrm{P} / \mathrm{A}^{(4)}$ |  | REF | IV2 ${ }^{(5}$ |  | 0 | 1 | 1 |
| $\mathrm{P} 0^{(6)}$ | RF synthesizer main divider coefficient |  |  |  |  |  |  |  |  |  |  |  |  |  | P15 | 0 | 0 | 0 |
| X | X | X | X | X | X | $\mathrm{R} 0^{(6)}$ | reference divider coefficient |  |  |  |  |  |  |  | R9 | 0 | 0 | 1 |
| X | X | A0 ${ }^{(6)}$ | IF synthesizer main divider coefficient |  |  |  |  |  |  |  |  |  |  |  | A13 | 0 | 1 | 0 |

## Notes

1. $X=$ don't care.
2. The test bits (at address 011) should not be programmed with any other value except all zeros for normal operation.
3. Bit XON = power-on of crystal oscillator low-noise amplifier; logic 1 turns on circuit block.
4. Bit $P / A=1$ selects the output of the reference subdivider to the RF synthesizer and the output of the common reference divider to the IF synthesizer.
5. The coefficient REFDIV2 (4 bits) selects the phase comparison ratio (1 to 16 ) between IF and RF synthesizers (see Table 2).
6. PO is the LSB of the RF main divider coefficient; RO is the LSB of the reference divider coefficient; A0 is the LSB of the IF main divider.

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Table 2 Programming the coefficient REFDIV2 for reference subdivider

| $\mathbf{d t 3}$ (LSB) | $\mathbf{d t 2}$ | $\mathbf{d t 1}$ | $\mathbf{d t 0}$ (MSB) | REFDIV2 |
| :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 0 | 0 | 1 |
| 1 | 0 | 0 | 0 | 2 |
| 0 | 1 | 0 | 0 | 3 |
| 1 | 1 | 0 | 0 | 4 |
| 0 | 0 | 1 | 0 | 5 |
| 1 | 0 | 1 | 0 | 6 |
| 0 | 1 | 1 | 0 | 7 |
| 1 | 0 | 1 | 0 | 8 |
| 0 | 1 | 0 | 1 | 9 |
| 1 | 1 | 0 | 1 | 10 |
| 0 | 0 | 0 | 1 | 11 |
| 1 | 0 | 1 | 1 | 12 |
| 0 | 1 | 1 | 1 | 13 |
| 0 | 1 | 1 | 1 | 14 |
| 1 | 1 | 1 | 15 |  |

Table 3 RF and IF synthesizer nominal charge pump currents (gain)

| CPI | SINGLE/DOUBLE | $\mathbf{I}_{\text {CPA }}(\mu \mathbf{A})$ | $\mathbf{I}_{\text {CPB }}(\mu \mathbf{A})$ |
| :---: | :---: | :---: | :---: |
| 0 | 0 | 470 | 470 |
| 0 | 1 | 840 | 840 |
| 1 | 0 | 1410 | 470 |
| 1 | 1 | 2480 | 840 |

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## LIMITING VALUES

In accordance with the Absolute Maximum Rating System (IEC 134).

| SYMBOL | PARAMETER | MIN. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{DD}}, \mathrm{V}_{\mathrm{DDX}}$ | digital and crystal reference supply voltages | -0.3 | +5.5 | V |
| $\mathrm{V}_{\text {CCA }}, \mathrm{V}_{\text {CCB }}$ | analog charge pump supply voltages | -0.3 | +5.5 | V |
| $\mathrm{V}_{\mathrm{C}}-\mathrm{V}_{\mathrm{D}}$ | difference in voltage between analog and digital supplies | -0.3 | +5.5 | V |
| $\mathrm{V}_{\mathrm{n}}$ | voltage <br> at pins $7,9,10,11$ and 13 <br> at pins 1,3 , and 20 <br> at pins 4 and 6 <br> at pins 15 and 17 | $\begin{aligned} & -0.3 \\ & -0.3 \\ & -0.3 \\ & -0.3 \end{aligned}$ | $\begin{aligned} & V_{\mathrm{DD}}+0.3 \\ & \mathrm{~V}_{\mathrm{DDX}}+0.3 \\ & \mathrm{~V}_{\mathrm{CCB}}+0.3 \\ & \mathrm{~V}_{\mathrm{CCA}}+0.3 \end{aligned}$ | $\begin{array}{\|l} \mathrm{V} \\ \mathrm{~V} \\ \mathrm{~V} \\ \mathrm{~V} \end{array}$ |
| $\Delta \mathrm{V}_{\mathrm{GND}}$ | difference in voltage between any of DGND, AGND and XGND (these pins should be connected together) | -0.3 | +0.3 | V |
| $\mathrm{P}_{\text {tot }}$ | total power dissipation | - | 120 | mW |
| $\mathrm{T}_{\text {stg }}$ | IC storage temperature | -55 | +125 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {amb }}$ | operating ambient temperature | -30 | +85 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\mathrm{j} \text { (max) }}$ | maximum junction temperature | - | 150 | ${ }^{\circ} \mathrm{C}$ |

## HANDLING

All pins withstand class 1 ESD test in accordance with "EIA/JESD22-A114-A" electrostatic discharge (ESD) sensitivity testing Human Body Model (HBM).

THERMAL CHARACTERISTICS

| SYMBOL | PARAMETER | CONDITIONS | VALUE | UNIT |
| :--- | :--- | :--- | :---: | :---: |
| $R_{\text {th } j-a}$ | thermal resistance from junction to ambient | in free air | 120 | K/W |

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## CHARACTERISTICS

All values refer to the typical measurement circuit; $\mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$; $\mathrm{V}_{\mathrm{DD}}=\mathrm{V}_{\mathrm{DDX}}=2.7$ to 5.5 V ; $\mathrm{V}_{\mathrm{CCA}}=\mathrm{V}_{\mathrm{CCB}}=2.7$ to 5.5 V ; $V_{C C A}=V_{C C B} \geq V_{D D}$; unless otherwise specified. Characteristics for which only a typical value is given are not tested.

| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Supplies; pins 5, 12, 16 and 19 |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{DD}}, \mathrm{V}_{\text {DDX }}$ | digital and crystal reference supply voltages | $\begin{aligned} & \mathrm{V}_{\mathrm{DD}}=\mathrm{V}_{\mathrm{DDX}} ; \\ & \mathrm{V}_{\mathrm{CCA}}=\mathrm{V}_{\mathrm{CCB}} \geq \mathrm{V}_{\mathrm{DD}} \end{aligned}$ | 2.7 | 3.0 | 5.5 | V |
| $\mathrm{V}_{\text {CCA }}, \mathrm{V}_{\text {CCB }}$ | charge pump supply voltages | $\mathrm{V}_{\text {CCA }}=\mathrm{V}_{\text {CCB }} \geq \mathrm{V}_{\text {DD }}$ | 2.7 | 3.0 | 5.5 | V |
| $\mathrm{I}_{\mathrm{DD}}$ | synthesizer digital supply current | $\begin{aligned} & \hline \mathrm{V}_{\mathrm{DD}}=3 \mathrm{~V} ; \overline{\mathrm{E}}=1 ; \\ & \mathrm{ON}_{\mathrm{A}} \text { and } \mathrm{ON} \\ & \mathrm{~B} \end{aligned}=1$ | - | 1.5 | 2.1 | mA |
| IDDX1 | reference block supply current | $\mathrm{V}_{\mathrm{DDX}}=3 \mathrm{~V} ; \mathrm{XON}=0$ | - | 0.25 | 0.4 | mA |
| IDDX2 | crystal oscillator and buffer currents | $\mathrm{V}_{\text {DDX }}=3 \mathrm{~V} ; \mathrm{XON}=1$ | - | 1.5 | 1.8 | mA |
| ICCA | RF synthesizer charge pump and prescaler supply currents | $\begin{aligned} & \hline \mathrm{V}_{\mathrm{CCA}}=3 \mathrm{~V} ; \\ & \mathrm{ON}_{\mathrm{A}} \text { and } \mathrm{ON}_{\mathrm{B}}=1 \end{aligned}$ | - | 8.1 | 9.8 | mA |
| $\mathrm{I}_{\text {CCB }}$ | IF synthesizer charge pump and prescaler supply currents | $\begin{aligned} & \hline \mathrm{V}_{\mathrm{CCB}}=3 \mathrm{~V} ; \\ & \mathrm{ON}_{\mathrm{A}} \text { and } \mathrm{ON}_{\mathrm{B}}=1 \end{aligned}$ | - | 4.8 | 5.7 | mA |
| $I_{\text {tot(pd) }}$ | total supply currents $\left(I_{C C A(p d)}+I_{D D(p d)}+I_{C C B(p d)}+I_{D D X(p d)}\right)$ in power-down mode | $\bar{E}=V_{D D} ; C L K$ and DATA $=0 \mathrm{~V}$ or $\mathrm{V}_{\mathrm{DD}}$; $\mathrm{ON}_{\mathrm{A}}$ and $\mathrm{ON}_{\mathrm{B}}=0$; $\mathrm{XON}=0$ | - | 40 | 80 | $\mu \mathrm{A}$ |
| RF main divider input; pin 15 |  |  |  |  |  |  |
| $\mathrm{f}_{\mathrm{RF}}$ | RF input frequency |  | 300 | - | 2100 | MHz |
| $\mathrm{V}_{\mathrm{RF}(\mathrm{rms})}$ | AC-coupled input signal level (RMS value) | $\mathrm{f}_{\mathrm{RF}}=600$ to 2100 MHz | 35 | - | 225 | mV |
|  |  | $\mathrm{f}_{\mathrm{RF}}=300$ to 600 MHz | 70 | - | 225 | mV |
| $\mathrm{R}_{\mathrm{m}}$ | main divider ratio |  | 512 | - | 65535 |  |
| $\mathrm{Z}_{\mathrm{i}}$ | input impedance (real part) | $\mathrm{f}_{\mathrm{RF}}=2 \mathrm{GHz}$ | - | 60 | - | $\Omega$ |
| $\mathrm{C}_{i}$ | pin input capacitance |  | - | 2 | - | pF |
| IF main divider input; pin 6 |  |  |  |  |  |  |
| $\mathrm{f}_{\mathrm{IF}}$ | IF input frequency | $\mathrm{V}_{\mathrm{CCA}}=\mathrm{V}_{\mathrm{CCB}} \leq 4.0 \mathrm{~V}$ | 50 | - | 550 | MHz |
|  |  |  | 50 | - | 400 | MHz |
| $\mathrm{V}_{\text {IF(rms) }}$ | AC-coupled input signal level (RMS value) | $\mathrm{f}_{\mathrm{IF}}=150$ to 550 MHz | 35 | - | 225 | mV |
|  |  | $\mathrm{f}_{\mathrm{IF}}=100$ to 150 MHz | 50 | - | 225 | mV |
|  |  | $\mathrm{f}_{\mathrm{IF}}=50$ to 100 MHz | 100 | - | 225 | mV |
| $\mathrm{R}_{\mathrm{m}}$ | main divider ratio |  | 128 | - | 16383 |  |
| $\mathrm{Z}_{\mathrm{i}}$ | input impedance (real part) | $\mathrm{f}_{\text {IF }}=400 \mathrm{MHz}$ | - | 60 | - | $\Omega$ |
| $\mathrm{C}_{i}$ | pin input capacitance |  | - | 2 | - | pF |

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| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Synthesizers reference divider input; pins 1 and 20 |  |  |  |  |  |  |
| $\mathrm{f}_{\text {xtal }}$ | crystal reference oscillator frequency |  | 3 | - | 20 | MHz |
| $\mathrm{V}_{\text {xtal(rms) }}$ | sinusoidal input signal level between pins 1 and 20 (RMS value) | $\begin{array}{\|l} \text { single-ended; } \\ f_{\text {xtal }}=6 \text { to } 20 \mathrm{MHz} \\ \mathrm{f}_{\mathrm{xtal}}=3 \text { to } 6 \mathrm{MHz} \end{array}$ | $\begin{aligned} & 35 \\ & 70 \end{aligned}$ | $\mid-$ | $\begin{array}{\|l} 250 \\ 250 \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{mV} \\ & \mathrm{mV} \end{aligned}$ |
|  |  | $\begin{array}{\|l} \text { differential; } \\ f_{\text {xtal }}=6 \text { to } 20 \mathrm{MHz} \\ \mathrm{f}_{\mathrm{xtal}}=3 \text { to } 6 \mathrm{MHz} \end{array}$ | $\begin{array}{\|l\|} 70 \\ 140 \end{array}$ | $\mid-$ | $\begin{array}{\|l} 500 \\ 500 \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{mV} \\ & \mathrm{mV} \end{aligned}$ |
| $\mathrm{R}_{\text {refc }}$ | common reference division ratio |  | 8 | - | 1023 |  |
| $\mathrm{R}_{\text {refa }}$ | reference subdivider division ratio |  | 1 | - | 16 |  |
| $\mathrm{Z}_{\mathrm{i}}$ | input impedance (real part) per pin | $\mathrm{f}_{\text {xtal }}=10 \mathrm{MHz} ; \mathrm{XON}=1$ | - | 4 | - | $\mathrm{k} \Omega$ |
| $\mathrm{C}_{i}$ | typical pin input capacitance |  | - | 2 | - | pF |
| NF | small signal differential input noise figure | matched to a $4 \mathrm{k} \Omega$ source; $\mathrm{XON}=1$ | - | 4.5 | - | dB |
| Phase detectors |  |  |  |  |  |  |
| $f_{\text {PCmax }}$ | maximum loop comparison frequency |  | - | 2000 | - | kHz |
| Charge pump outputs; pins 4 and 17 |  |  |  |  |  |  |
| $\mathrm{V}_{\text {CPA }}$ | output voltage compliance range; RF synthesizer |  | 0.4 | - | $\mathrm{V}_{\text {CCA }}-0.4$ | V |
| $\mathrm{V}_{\text {CPB }}$ | output voltage compliance range; IF synthesizer |  | 0.4 | - | $\mathrm{V}_{\text {CCB }}-0.4$ | V |
| $\mathrm{I}_{\text {ocp(err) }}$ | charge pump output current error | note 1 | -25 | - | +25 | \% |
| $I_{\text {match }}$ | sink-to-source current matching |  | - | $\pm 5$ | - | \% |
| $\mathrm{l}_{\text {Lcp }}$ | charge pump off leakage current | $\begin{aligned} & \mathrm{V}_{\mathrm{CPA}}=1 / 2 \mathrm{~V}_{\mathrm{CCA}} ; \\ & \mathrm{V}_{\mathrm{CPB}}=1 / 2 \mathrm{~V}_{\mathrm{CCB}} \\ & \hline \end{aligned}$ | -5 | $\pm 1$ | +5 | nA |
| Phase noise |  |  |  |  |  |  |
| $\mathrm{N}_{900}$ | RF synthesizer's contribution to close-in phase noise of 0.9 GHz VCO signal inside closed-loop bandwidth | $\begin{array}{\|l} \hline \mathrm{f}_{\text {xtal }}=13 \mathrm{MHz} ; \\ \mathrm{V}_{\mathrm{xtal}}=0 \mathrm{dBm} ; \\ \mathrm{f}_{\mathrm{PC}}=200 \mathrm{kHz} \\ \hline \end{array}$ | - | -86 | - | dBc/Hz |
| $\mathrm{N}_{1800}$ | RF synthesizer's contribution to close-in phase noise of 1.8 GHz VCO signal inside closed-loop bandwidth | $\begin{array}{\|l\|} \hline \mathrm{f}_{\mathrm{xtal}}=13 \mathrm{MHz} ; \\ \mathrm{V}_{\mathrm{xtal}}=0 \mathrm{dBm} ; \\ \mathrm{f}_{\mathrm{PC}}=200 \mathrm{kHz} \\ \hline \end{array}$ | - | -80 | - | dBc/Hz |
| $\mathrm{N}_{180}$ | IF synthesizer's contribution 180 MHz VCO signal inside closed-loop bandwidth | $\begin{aligned} & \hline \mathrm{f}_{\mathrm{xtal}}=13 \mathrm{MHz} ; \\ & \mathrm{V}_{\mathrm{xtal}}=0 \mathrm{dBm} ; \\ & \mathrm{f}_{\mathrm{PC}}=1000 \mathrm{kHz} \end{aligned}$ | - | -104 | - | dBc/Hz |

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 radio telephones| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interface logic input signal levels; pins 7, 9, 10, 11 and 13 |  |  |  |  |  |  |
| $\mathrm{V}_{\text {IH }}$ | HIGH-level input voltage |  | $0.7 \mathrm{~V}_{\mathrm{DD}}$ | - | $V_{D D}+0.3$ | V |
| $\mathrm{V}_{\text {IL }}$ | LOW-level input voltage |  | -0.3 | - | $0.3 V_{D D}$ | V |
| $\mathrm{I}_{\text {bias }}$ | input bias current | logic 1 or logic 0 | -5 | - | +5 | $\mu \mathrm{A}$ |
| $\mathrm{C}_{\mathrm{i}}$ | input capacitance |  | - | 2 | - | pF |
| Low noise crystal oscillator amplifier output signals; pins 3 and 18 |  |  |  |  |  |  |
| Z | differential output impedance (real part) | $\mathrm{f}_{\text {xtal }}=10 \mathrm{MHz}$ | - | 2 | - | $\mathrm{k} \Omega$ |
| V Xout, <br> V Xoutn | DC output voltage |  | - | 2.29 | - | V |
| $\mathrm{G}_{\mathrm{v} \text { (diff) }}$ | small signal differential voltage gain | XON = 1; $\mathrm{f}_{\text {xtal }}=10 \mathrm{MHz}$ | 18 | 20 | 22 | dB |
| $\mathrm{V}_{0(p-p)}$ | limiting differential output voltage swing (peak-to-peak value) | $\mathrm{XON}=1$ | - | 2 | - | V |
| $\Delta f / f\left(\mathrm{~V}_{\mathrm{DDX}}\right)$ | frequency stability as a function of supply voltage change (referenced to initial frequency) | $\mathrm{V}_{\text {DDX }}=3 \mathrm{~V} \pm 5 \%$; note 2 | - | $\pm 0.25$ | - | ppm |
| System specification |  |  |  |  |  |  |
| $\mathrm{FTRF}_{\text {IF }}$ | RF frequency and close harmonics feedthrough to IF frequency | note 3 | - | 70 | - | dBc |
| $\mathrm{FTIF}_{\text {RF }}$ | IF frequency and close harmonics feedthrough to RF frequency | note 3 | - | 50 | - | dBc |

## Notes

1. Conditions: $0.4<\mathrm{V}_{\mathrm{CPA}}<\left(\mathrm{V}_{\mathrm{CCA}}-0.4\right)$ and $0.4<\mathrm{V}_{\mathrm{CPB}}<\left(\mathrm{V}_{\mathrm{CCB}}-0.4\right)$.
2. This value is directly dependent on the external resonator quality factor. Only guaranteed for the application circuit which is given in Fig. 5 .
3. Only guaranteed on the Philips application board.

## Low cost dual frequency synthesizer for radio telephones

## SERIAL BUS TIMING CHARACTERISTICS

$\mathrm{V}_{\mathrm{DD}}=\mathrm{V}_{\mathrm{DDX}}=\mathrm{V}_{\mathrm{CCA}}=\mathrm{V}_{\mathrm{CCB}}=3 \mathrm{~V} ; \mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$; unless otherwise specified.

| SYMBOL | PARAMETER | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Serial programming clock; CLK |  |  |  |  |  |
| $\mathrm{t}_{\mathrm{r}}$ | input rise time | - | 10 | 40 | ns |
| $\mathrm{t}_{\mathrm{f}}$ | input fall time | - | 10 | 40 | ns |
| $\mathrm{T}_{\text {cy }}$ | clock period | 100 | - | - | ns |
| Enable programming; $\overline{\mathbf{E}}$ |  |  |  |  |  |
| tstart | delay to rising clock edge | 100 | - | - | ns |
| $\mathrm{t}_{\text {END }}$ | delay from last falling clock edge | 20 | - | - | ns |
| $\mathrm{t}_{\mathrm{W} \text { (min) }}$ | minimum inactive pulse width | 1500(1) | - | - | ns |
| tsu;E | enable set-up time to next clock edge | 20 | - | - | ns |
| Register serial input data; DATA |  |  |  |  |  |
| $\mathrm{t}_{\text {SU; }}$ DAT | input data to clock set-up time | 20 | - | - | ns |
| $\mathrm{t}_{\text {HD; DAT }}$ | input data to clock hold time | 20 | - | - | ns |

## Note

1. The minimum pulse width $\left(\mathrm{t}_{\mathrm{w}(\text { min })}\right)$ can be smaller than $1.5 \mu \mathrm{~s}$ when the following conditions are fulfilled:
a) Main divider input frequency $f_{R F}>\frac{383}{t_{W(\text { min })}}$
b) Reference divider input frequency $f_{x t a l}>\frac{3}{t_{W(\text { min })}}$


## Low cost dual frequency synthesizer for radio telephones

## AC TIMING CHARACTERISTICS

$\mathrm{V}_{\mathrm{DD}}=\mathrm{V}_{\mathrm{DDX}}=\mathrm{V}_{\mathrm{CCA}}=\mathrm{V}_{\mathrm{CCB}}=3 \mathrm{~V} ; \mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$; unless otherwise specified.

| SYMBOL | PARAMETER | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| tPup | delay for initial power-up | - | 400 | - | $\mu \mathrm{S}$ |
| tPDWN | time for power-down from $\overline{\mathrm{E}}=0\left(\mathrm{ON}_{\mathrm{A}} / \mathrm{ON}_{\mathrm{B}}=0\right)$ | - | 100 | - | $\mu \mathrm{s}$ |
| tstart | time to turn-on either the RF or IF synthesizer from $\mathrm{ON}_{\mathrm{A}} / \mathrm{ON}_{\mathrm{B}}$ | - | 50 | - | $\mu \mathrm{S}$ |
| $t_{\text {END }}$ | time to turn-off either the RF or IF synthesizer from $\mathrm{ON}_{\mathrm{A}} / \mathrm{ON}_{\mathrm{B}}$ | - | 70 | - | $\mu \mathrm{s}$ |
| tsend | waiting time before sending data on the serial bus | 15000 | - | - | $\mu \mathrm{s}$ |



## Low cost dual frequency synthesizer for

 radio telephones
## APPLICATION INFORMATION


(1) Loop filter values depend on the application.

Fig. 5 Typical test and application diagram.

Low cost dual frequency synthesizer for radio telephones


## Low cost dual frequency synthesizer for

UMA1022M radio telephones

## PACKAGE OUTLINE



DIMENSIONS (mm are the original dimensions)

| UNIT | $\mathbf{A}$ <br> max. | $\mathbf{A}_{\mathbf{1}}$ | $\mathbf{A}_{\mathbf{2}}$ | $\mathbf{A}_{\mathbf{3}}$ | $\mathbf{b}_{\mathbf{p}}$ | $\mathbf{c}$ | $\mathbf{D}^{(1)}$ | $\mathbf{E}^{(1)}$ | $\mathbf{e}$ | $\mathbf{H}_{\mathbf{E}}$ | $\mathbf{L}$ | $\mathbf{L}_{\mathbf{p}}$ | $\mathbf{Q}$ | $\mathbf{v}$ | $\mathbf{w}$ | $\mathbf{y}$ | $\mathbf{Z}^{(\mathbf{1})}$ | $\boldsymbol{\theta}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm | 1.5 | 0.15 <br> 0 | 1.4 | 0.2 | 1.2 | 0.32 | 0.20 <br> 0.20 <br> 0.13 | 6.6 <br> 6.4 | 4.5 <br> 4.3 | 0.65 | 6.6 <br> 6.2 | 1.0 | 0.75 <br> 0.45 | 0.65 <br> 0.45 | 0.2 | 0.13 | 0.1 | 0.48 <br> 0.18 |

Note

1. Plastic or metal protrusions of 0.20 mm maximum per side are not included.


## Low cost dual frequency synthesizer for radio telephones

## SOLDERING

## Introduction to soldering surface mount packages

This text gives a very brief insight to a complex technology. A more in-depth account of soldering ICs can be found in our "Data Handbook IC26; Integrated Circuit Packages" (document order number 9398652 90011).

There is no soldering method that is ideal for all surface mount IC packages. Wave soldering is not always suitable for surface mount ICs, or for printed-circuit boards with high population densities. In these situations reflow soldering is often used.

## Reflow soldering

Reflow soldering requires solder paste (a suspension of fine solder particles, flux and binding agent) to be applied to the printed-circuit board by screen printing, stencilling or pressure-syringe dispensing before package placement.

Several methods exist for reflowing; for example, infrared/convection heating in a conveyor type oven.
Throughput times (preheating, soldering and cooling) vary between 100 and 200 seconds depending on heating method.

Typical reflow peak temperatures range from 215 to $250^{\circ} \mathrm{C}$. The top-surface temperature of the packages should preferable be kept below $230^{\circ} \mathrm{C}$.

## Wave soldering

Conventional single wave soldering is not recommended for surface mount devices (SMDs) or printed-circuit boards with a high component density, as solder bridging and non-wetting can present major problems.

To overcome these problems the double-wave soldering method was specifically developed.

If wave soldering is used the following conditions must be observed for optimal results:

- Use a double-wave soldering method comprising a turbulent wave with high upward pressure followed by a smooth laminar wave.
- For packages with leads on two sides and a pitch (e):
- larger than or equal to 1.27 mm , the footprint longitudinal axis is preferred to be parallel to the transport direction of the printed-circuit board;
- smaller than 1.27 mm , the footprint longitudinal axis must be parallel to the transport direction of the printed-circuit board.

The footprint must incorporate solder thieves at the downstream end.

- For packages with leads on four sides, the footprint must be placed at a $45^{\circ}$ angle to the transport direction of the printed-circuit board. The footprint must incorporate solder thieves downstream and at the side corners.

During placement and before soldering, the package must be fixed with a droplet of adhesive. The adhesive can be applied by screen printing, pin transfer or syringe dispensing. The package can be soldered after the adhesive is cured.

Typical dwell time is 4 seconds at $250^{\circ} \mathrm{C}$.
A mildly-activated flux will eliminate the need for removal of corrosive residues in most applications.

## Manual soldering

Fix the component by first soldering two diagonally-opposite end leads. Use a low voltage ( 24 V or less) soldering iron applied to the flat part of the lead. Contact time must be limited to 10 seconds at up to $300^{\circ} \mathrm{C}$.

When using a dedicated tool, all other leads can be soldered in one operation within 2 to 5 seconds between 270 and $320^{\circ} \mathrm{C}$.

Low cost dual frequency synthesizer for radio telephones

Suitability of surface mount IC packages for wave and reflow soldering methods

| PACKAGE | SOLDERING METHOD |  |
| :---: | :---: | :---: |
|  | WAVE | REFLOW ${ }^{(1)}$ |
| BGA, SQFP <br> HLQFP, HSQFP, HSOP, HTSSOP, SMS <br> PLCC ${ }^{(3)}$, SO, SOJ <br> LQFP, QFP, TQFP <br> SSOP, TSSOP, VSO | not suitable <br> not suitable ${ }^{(2)}$ <br> suitable <br> not recommended ${ }^{(3)(4)}$ <br> not recommended(5) | suitable <br> suitable <br> suitable <br> suitable <br> suitable |

## Notes

1. All surface mount (SMD) packages are moisture sensitive. Depending upon the moisture content, the maximum temperature (with respect to time) and body size of the package, there is a risk that internal or external package cracks may occur due to vaporization of the moisture in them (the so called popcorn effect). For details, refer to the Drypack information in the "Data Handbook IC26; Integrated Circuit Packages; Section: Packing Methods".
2. These packages are not suitable for wave soldering as a solder joint between the printed-circuit board and heatsink (at bottom version) can not be achieved, and as solder may stick to the heatsink (on top version).
3. If wave soldering is considered, then the package must be placed at a $45^{\circ}$ angle to the solder wave direction. The package footprint must incorporate solder thieves downstream and at the side corners.
4. Wave soldering is only suitable for LQFP, TQFP and QFP packages with a pitch (e) equal to or larger than 0.8 mm ; it is definitely not suitable for packages with a pitch (e) equal to or smaller than 0.65 mm .
5. Wave soldering is only suitable for SSOP and TSSOP packages with a pitch (e) equal to or larger than 0.65 mm ; it is definitely not suitable for packages with a pitch (e) equal to or smaller than 0.5 mm .

## DEFINITIONS

| Data sheet status |  |
| :--- | :--- |
| Objective specification | This data sheet contains target or goal specifications for product development. |
| Preliminary specification | This data sheet contains preliminary data; supplementary data may be published later. |
| Product specification | This data sheet contains final product specifications. |
| Limiting values | Limiting values given are in accordance with the Absolute Maximum Rating System (IEC 134). Stress above one or <br> more of the limiting values may cause permanent damage to the device. These are stress ratings only and operation <br> of the device at these or at any other conditions above those given in the Characteristics sections of the specification <br> is not implied. Exposure to limiting values for extended periods may affect device reliability. |
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