

L4915

ADJUSTABLE VOLTAGE REGULATOR PLUS FILTER

PRELIMINARY DATA

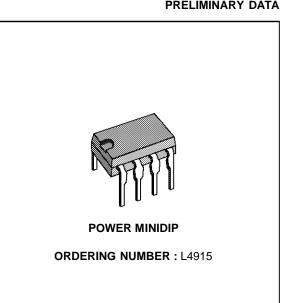
- OUTPUT VOLTAGE ADJUSTABLE FROM 4 TO 11V
- HIGH OUTPUT CURRENT (up to 250mA)
- HIGH RIPPLE REJECTION
- HIGH LOAD REGULATION
- HIGH LINE REGULATION
- SHORT CIRCUIT PROTECTION
- THERMAL SHUT DOWN WITH HYSTERESIS
- DUMP PROTECTION

DESCRIPTION

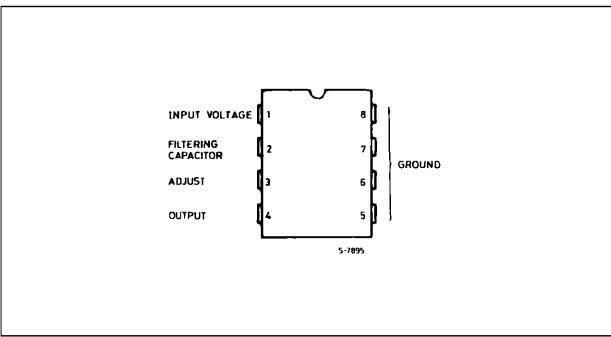
This circuit combines both a filter and a voltage regulator in order to provide a high ripple rejection over a wide input voltage range.

A supervisor low-pass loop of the element prevents the output transistor from saturation at low input voltage.

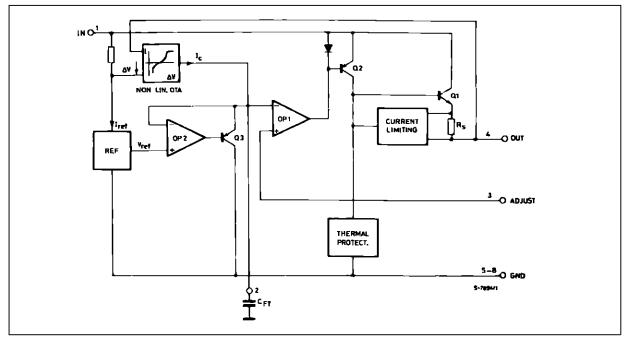
The non linear behaviour of this control circuitry allows a fast settling of the filter.



PIN CONNECTION



BLOCK DIAGRAM



ABSOLUTE MAXIMUM RATINGS

Symbol	Parameter	Value	Unit
Vi	Peak Input Voltage (300 ms)	40	V
Vi	DC Input Voltage	28	V
lo	Output Current	Internally Limited	
Ptot	Power Dissipation	Internally Limited	
T _{stg}	Storage and Junction Temperature	– 40 to 150	°C

THERMAL DATA

Symbol	Parameter	Value	Unit
R _{th j-amb}	Thermal Resistance Junction-ambient Max.	80	°C/W
R _{th} j-pins	Thermal Resistance Junction-pins Max.	20	°C/W

ELECTRICAL CHARACTERISTICS

 $(T_{amb} = 25^{\circ}C; V_i = 13.5 V, V_O = 8.5V, circuit of Fig. 1, unless otherwise specified)$

Symbol	Parameter Test Conditions		Min.	Тур.	Max.	Unit
Vi	Input Voltage				20	V
Vo	Output Voltage	$V_i = 6 \text{ to } 18V, I_o = 5 \text{ to } 150\text{mA}$	4		11	V
$\Delta V_{I/O}$	Controlled Input-output Dropout Voltage	$I_0 = 5$ to 150mA, $V_i = 6$ to 10V		1.6	2.1	V
ΔV_O	Line Regulation	$V_i = 12 \text{ to } 18V, I_o = 10\text{mA}$		1	20	mV
ΔV_{o}	Load Regulation	$ I_o = 5 \text{ to } 250 \text{mA}, \\ t_{on} = 30 \mu \text{s}, t_{off} = \geq 1 \text{ms} $		50	100	mV
ΔV_{o}	Load Regulation (filter mode)	$\begin{array}{l} V_i = 8.5V, \ I_o = 5 \ to \ 150 mA \\ t_{on} = 30 \mu s, \ t_{off} = \ge 1 ms \end{array}$		150	250	mV
V _{ref}	Internal Voltage Reference			2.5		V
Ιq	Quiescent Current	$I_0 = 5 \text{ mA}$		1	2	mA
Δl_q	Quiescent Current Change	$V_i = 6 \text{ to } 18V, I_0 = 5 \text{ to } 150\text{mA}$		0.05		mA
I _{AD}	Adjust Input Current			40		nA



ELECTRICAL CHARACTERISTICS (continued)

(T_{amb} = 25°C; V_i = 13.5 V, V_O = 8.5V, circuit of Fig. 1, unless otherwise specified)

Symbol	Parameter	Test Conditions	Min.	Тур.	Max.	Unit
$\frac{\Delta V_{O}}{\Delta T}$	Output Voltage Drift	I _o = 10mA		1.2		mV/°C
SVR	Supply Voltage Rejection	$V_{iac} = 1V_{RMS}, f = 100Hz, I_o = 150mA$ Regulator Filter Mode		71 35(*)		dB
Isc	Short Circuit Current		250	300		mA
Ton	Switch On Time	l _o = 150mA Regulator Filter Mode		300 500(*)		ms
Tj	Thermal Shutdown Junction Temperature			145		°C

(*) Depending of the CFT capacitor

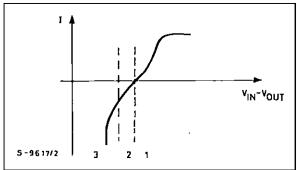
PRINCIPLE OF OPERATION

During normal operation (input voltage upper than $V_{I MIN} = V_{OUT NOM} + \Delta V_{I/O}$). The device works as a normal voltage regulator built around the OP1 of the block diagram.

The series pass element uses a PNP-NPN connection to reduce the dropout. The reference voltage of the OP1 is derived from a REF through the OP2 and Q3, acting as an active zener diode of value VRFF.

In this condition the device works in the range (1) of the characteristic of the non linear drop control unit (see Figure 1).





The output voltage is fixed to its nominal value :

$$V_{OUT NOM} = V_{REF} \left(1 + \frac{R1}{R2} \right) = V_{CFT} \left(1 + \frac{R1}{R2} \right)$$

The ripple rejection is guite high (70dB) and independent to CFT value.

On the usual voltage regulators, when the input vol-tage goes below the nominal value, the regulation transistors (series element) saturate bringing the system out of regulation and making it very sensible to every variation of the input voltage. On the contrary, a control loop on the L4915 consents to avoid the saturation of the series element by regulating the value of the reference voltage (pin 2). In fact, whenever the input voltage decreases below (VI MIN the supervisor loop, utilizing a non linear OTA, forces the reference voltage at pin 2 to decrease by discharging C_{FT}. So, during the static mode, when the input voltage goes below V_{MIN} the drop out is kept fixed to about 1.6 V. In this condition the device works as a low pass filter in the range (2) of the OTA characteristic. The ripple rejection is externally adjustable acting on CFT as follows:

$$SVR (j\Omega) = \left| \frac{V_i(j\Omega)}{V_{OUT}(j\Omega)} \right| = 1 + \left| \frac{10^{-6}}{\frac{gm}{jw C_{FT}} \left(1 + \frac{R1}{R2} \right)} \right|$$

Where:

gm =
$$2 \cdot 10^{-5} \Omega^{-1}$$

= OTA'S typical transconductance value on
linear region

 C_{FT} = value of capacitor in μF

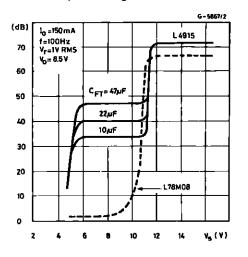
The reaction time of the supervisor loop is given by the transconductance of the OTA and by CFT. When the value of the ripple voltage is so high and its negative peak is fast enough to determine an istantaneous decrease of the dropout till 1.2V, the OTA works in a higher transconductance condition [range (3) of the characteristic] and discharges the capacitor rapidously.

If the ripple frequency is high enough the capacitor won't charge itself completely, and the output voltage reaches a small value allowing a better ripple rejection; the device's again working as a filter (fast transient range).

With $C_{FT} = 10\mu F$; f = 100Hz; $V_0 = 8.5V \text{ a SVR of } 35$ is obtained.



Figure 2 : Supply Voltage Rejection versus Input Voltage





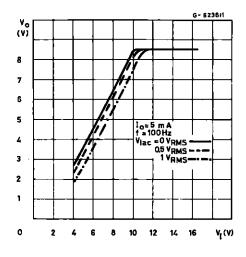


Figure 6 : Dropout versus Load Current

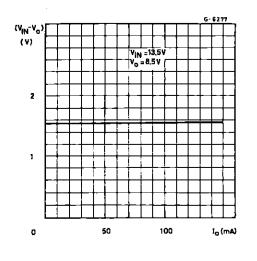


Figure 3 : Supply Voltage Rejection versus Frequency

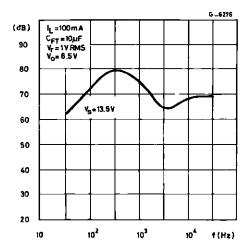
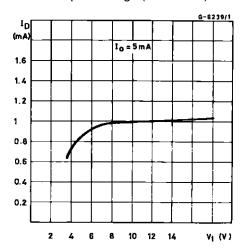
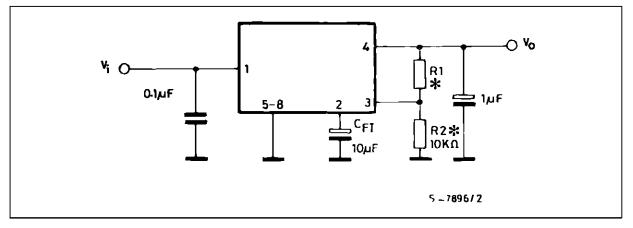


Figure 5 : Quiescent Current versus Input Voltage (V_O = 8.5V)





APPLICATION CIRCUIT

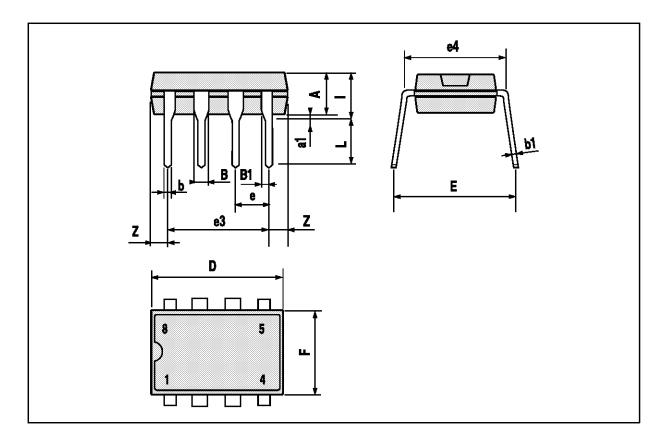




L4915

DIM.	mm					
Dim.	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.
А		3.3			0.130	
a1	0.7			0.028		
В	1.39		1.65	0.055		0.065
B1	0.91		1.04	0.036		0.041
b		0.5			0.020	
b1	0.38		0.5	0.015		0.020
D			9.8			0.386
E		8.8			0.346	
е		2.54			0.100	
e3		7.62			0.300	
e4		7.62			0.300	
F			7.1			0.280
I			4.8			0.189
L		3.3			0.130	
Z	0.44		1.6	0.017		0.063

MINIDIP 4+4 PACKAGE MECHANICAL DATA





Information furnished is believed to be accurate and reliable. However, SGS-THOMSON Microelectronics assumes no responsibility for the consequences of use of such information nor for any infringement of patents or other rights of third parties which may result from its use. No license is granted by implication or otherwise under any patent or patent rights of SGS-THOMSON Microelectronics. Specifications mentioned in this publication are subject to change without notice. This publication supersedes and replaces all information previously supplied. SGS-THOMSON Microelectronics products are not authorized for use as critical components in life support devices or systems without express written approval of SGS-THOMSON Microelectronics.

© 1994 SGS-THOMSON Microelectronics - All Rights Reserved

SGS-THOMSON Microelectronics GROUP OF COMPANIES

Australia - Brazil - France - Germany - Hong Kong - Italy - Japan - Korea - Malaysia - Malta - Morocco - The Netherlands - Singapore -Spain - Sweden - Switzerland - Taiwan - Thaliand - United Kingdom - U.S.A.

