## SMOOTH DRIVE SPINDLE MOTOR FOR OPTICAL DRIVE APPLICATION WITH POWER INTEGRATED

- SMOOTH DRIVE™ SYSTEM
- 1.8A DRIVE PEAK CAPABILITY
- SLEW RATE CONTROL
- INDUCTIVE SENSE START-UP ROUTINE
- THERMAL SHUTDOWN
- SUITABLE FOR 5V AND 12V APPLICATION
- ONLY ONE HALL SENSOR IS REQUIRED


## DESCRIPTION

The L7203 SPINDLE MOTOR IC includes a three phase brushless spindle motor controller and the power stage in switching mode. The device is designed for both 5V and 12V OPTICAL DRIVE application requiring up to 1.8A peak of current.
The device is realized in BCD5, a $0.7 \mu \mathrm{~m}$ Mixed technology.
The spindle motor position detection is carried out by means of a single comparator with hysteresis. In the start-up phase the "inductive sense

start up method" is used to detect the rotor position, determining the direction of starting rotation. This procedure is implemented by a logic circuit on chip.
The device applies three sinusoidal voltages to the motor coils.
This is obtained through the application of the

## BLOCK DIAGRAM



DESCRIPTION (continued)
SMOOTH DRIVING concept.
It is based on the idea of driving the motor winding through 3 sinusoidal voltages dephased of 120 degrees. The motor is controlled in voltage mode, so no current control compensation network is required.
Each profile is digitally described by 36 bytes stored in a ROM memory.
These sinusoidal signals are modulated by multiplying each sample by a value stored in the KVAL register. Using this kind of profiles it is possible to obtain great advantages such as torque ripple and acoustic noise reduction and lower EMI. An easier track following is ensured, since vibration are reduced.
The clock signal on the chip can be synchronized to the external application clock signal.
An internal circuit can limit the current. The threshold is fixed with a internal 0.2 V reference.

The device generates:

- a current generator to define output voltage slew rate
- a 3.3 V reference to bias hall sensor.
- the HFG open drain output signal for speed regulation.
The device includes:
- a circuit for thermal shutdown with hysteresis.
- a low voltage detector

In the STANDBY state the main functions of the device are turned off, in order to minimize the power consumption.

The STANDBY state of the device is imposed by:

- Thermal shutdown
- stand by signal from $\mu \mathrm{P}$


## PIN CONNECTIONS



## PIN DESCRIPTION

| PIN | DESCRIPTION | TYPE |
| :---: | :--- | :---: |
| POWER AND GROUND | P12 |  |
| VM | Supply voltage for power stages +12/5V | P5 |
| VCC | Supply for 5V core | G |
| DGND | Logic ground | G |
| AGND | Analog ground | IC5 |
| DIGITAL PIN | IC5 |  |
| PWMIN | PWM input signal to calculate kval | IC5 |
| Fsys | System frequency | IC5 |
| PHS | Phase Shift Pin | ZD5 |
| PRS | Prescaler Pin | OD5 |
| STB | Start and Stop signal | OA5 |
| HFG | Open Drain F-Generator signal from Spindle Motor | IA5 |
| HALL SENSOR |  |  |
| BIAS | 3.3V reference to bias Hall sensor | IA5 |
| H+, H- | Hall sensor differential input | OA12 |
| INDUCTIVE SENSE REFERENCE | OA12 |  |
| ISR | Inductive sense reference | OA12 |
| MOTOR CONTROL | OA12 |  |
| OUTV | Winding output U | IA5 |
| OUTV | Winding output V | OA5 |
| OUTW | Winding output W |  |
| RF | Current sense resistor (force) |  |
| RF1 | Current sense resistor (sense) |  |
| SLEW RATE CONTROL | Slew Rate Control |  |
| SRC |  |  |

## INPUT DEFINITION

IC5 Input CMOS, 3.3-5V capability with hysteresis
ZD5 Bidirectional, open drain, $3.3-5 \mathrm{~V}$ capability
OD5 Output, open drain, $3.3-5 \mathrm{~V}$ capability
IA5 Input, Analog, 5V
OA5 Output, Analog, 5V
OA12 Output, Analog, 12V
P12 Power 12V / 5V
P5 Power 5V
G Ground

## THERMAL DATA

| Symbol | Parameter | Value | Unit |  |
| :---: | :--- | :---: | :---: | :---: |
| $\mathrm{R}_{\text {th } \mathrm{j} \text {-pins }}$ | Thermal Resistance Junction to Pins | Max. | 16 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\mathrm{R}_{\text {th } \mathrm{j} \text {-amb }}$ | Thermal Resistance Junction to Ambient | Max. | 90 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

## ABSOLUTE MAXIMUM RATINGS

| Symbol | Parameter | Value | Unit |
| :---: | :---: | :---: | :---: |
| $\mathrm{T}_{\text {amb }}$ | Ambient Temperature | -20 to 80 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {op }}$ | Operating Temperature | 0 to 150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {smin }}$ | Minimum Thermal Circuit Threshold | 140 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{V}_{\mathrm{M}}$ |  | -0.3 to 15 | Vdc |
| $\mathrm{V}_{\mathrm{CC}}$ |  | -0.3 to 7 | Vdc |
|  | U, V, W, (low side drive =off) | -0.3 to 17 | Vdc |
|  | PWMIN, PHS, FSYS, TEST, STB, HFG, BIAS, H+, H-, RF1, RF, ISR, PORPin | -0.3 to $\mathrm{V}_{\mathrm{Cc}}+0.3$ | Vdc |
| $\mathrm{P}_{\mathrm{D} 1}$ | Power dissipation at sustained operation with a package $R_{t h j}$-amb at $90^{\circ} \mathrm{C}$ | 1 | W |
| ESD | Susceptibility | 2000 | Vac |
| TSTG | Storage Temperature | -55 to 150 | ${ }^{\circ} \mathrm{C}$ |
| IOLHFG | HFG open drain current | 10 | mA |
| $\mathrm{l}_{\text {Peak }}$ | Motor Peak Current | 1.8 | A |

DC ELECTRICAL CHARACTERISTICS ( $\mathrm{VcC}=5 \mathrm{~V} ; \mathrm{V}_{\mathrm{M}}=12 \mathrm{~V}$; Tamb $=25^{\circ} \mathrm{C}$ unless otherwise specified)

\begin{tabular}{|c|c|c|c|c|c|c|}
\hline Symbol \& Parameter \& Test Condition \& Min. \& Typ. \& Max. \& Unit <br>
\hline \multicolumn{7}{|l|}{SUPPLY} <br>
\hline $\mathrm{V}_{\mathrm{CC}}$ \& Supply 5V operating range \& \& 4.25 \& \& 5.75 \& V <br>
\hline $\mathrm{V}_{\mathrm{M}}$ \& Supply 12 V operating range \& (note 1) \& 10.2 \& \& 13.8 \& V <br>
\hline $\mathrm{V}_{\mathrm{M}}$ \& Supply 5V operating range \& \& 4.25 \& \& 5.75 \& V <br>
\hline $\mathrm{I}_{\mathrm{Vcc}}$ \& Vcc Supply Current \& $$
\begin{array}{ll}
\hline V_{c c}=5.75 ; f_{\text {sys }}=20 M H z ~ S T B ~ & =0 \\
\text { (bias pin open) } & \text { STB }=1 \\
\hline
\end{array}
$$ \& \& \& $$
\begin{aligned}
& 1.3 \\
& 20 \\
& \hline
\end{aligned}
$$ \& $$
\begin{aligned}
& \mathrm{mA} \\
& \mathrm{~mA}
\end{aligned}
$$ <br>
\hline $\mathrm{V}_{\mathrm{Vm}}$ \& VM Supply Current \& $\mathrm{V}_{\mathrm{M}}=13.8$

$\begin{aligned} & \text { STB }=0 \\ & \text { STB }\end{aligned}$ \& \& \& 1 \& $$
\begin{aligned}
& \hline \mathrm{mA} \\
& \mathrm{~mA}
\end{aligned}
$$ <br>

\hline \multicolumn{7}{|l|}{PWMIN, PHS, PRS, Fsys} <br>
\hline $\mathrm{V}_{\mathrm{iL}}$ \& Input Low Voltage \& \& \& \& 1 \& V <br>
\hline $\mathrm{V}_{\mathrm{iH}}$ \& Input High Voltage \& \& 2.2 \& \& \& V <br>
\hline $\mathrm{V}_{\mathrm{iHYS}}$ \& Input Hysteresis \& \& \& 100 \& \& mV <br>
\hline $\mathrm{I}_{2}$ \& Leakage Current \& $V_{C C}=5.75$ \& -10 \& \& +10 \& $\mu \mathrm{A}$ <br>
\hline \multicolumn{7}{|l|}{STB} <br>
\hline $\mathrm{V}_{\mathrm{iL}}$ \& Input Low Voltage \& \& \& \& 1 \& V <br>
\hline $\mathrm{V}_{\mathrm{iH}}$ \& Input High Voltage \& \& 2.2 \& \& \& V <br>
\hline VoL \& Open Drain Output \& $\mathrm{IOL}=2 \mathrm{~mA} \mathrm{~V} \mathrm{CC}=4.25 \mathrm{~V}$ \& \& \& 0.4 \& V <br>
\hline $\mathrm{V}_{\mathrm{iHYS}}$ \& Input Hysteresis \& \& \& 100 \& \& mV <br>
\hline $\mathrm{I}_{2}$ \& Leakage Current \& $\mathrm{V}_{\mathrm{CC}}=5.75$, Therm off \& -10 \& \& +10 \& $\mu \mathrm{A}$ <br>
\hline \multicolumn{7}{|l|}{HFG} <br>
\hline VOL \& Open Drain Output \& $\mathrm{IOL}=2 \mathrm{~mA} \quad \mathrm{~V}_{\mathrm{CC}}=5 \mathrm{~V}$ \& \& \& 0.4 \& V <br>
\hline $\mathrm{I}_{2}$ \& Leakage Current \& $\mathrm{V}_{\text {CC }}=5.75$, HFG hiz \& -10 \& \& +10 \& $\mu \mathrm{A}$ <br>
\hline
\end{tabular}

DC ELECTRICAL CHARACTERISTICS (continued)

| Symbol | Parameter | Test Condition | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BIAS |  |  |  |  |  |  |
| $\mathrm{V}_{\text {BIAS }}$ | BIAS Output Voltage | $\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V} ; 5 \mathrm{~mA}<\mathrm{l}<15 \mathrm{~mA}$ | 3.25 |  | 3.75 | V |
| $I_{\text {Bmax }}$ | Max Output Current |  |  |  | 15 | mA |
| $\mathrm{H}+$, $\mathrm{H}-$ |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{H}+}$ | H+ H- Input Voltage Range |  | 0 |  | 2.5 | V |
| $\mathrm{l}_{\mathrm{H} \pm}$ | Input Leakage Current | V in $=0,+\mathrm{Vcc}$ | -10 |  | +10 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {OFFISR }}$ | Comparator Offset |  | -15 |  | +15 | mV |
| VHy | Comparator Hysteresys |  | 4 |  | 15 | mV |
| MOTOR POWER STAGE |  |  |  |  |  |  |
| $\mathrm{R}_{\text {DSON }}$ | High and Low side FET on Resistance | $\begin{aligned} & \mathrm{T}_{\mathrm{j}}=125 ; \quad \mathrm{V}_{\mathrm{M}}=4.25 \mathrm{~V} \\ & \mathrm{I}=1.2 \mathrm{~A} \end{aligned}$ |  |  | 2 | $\Omega$ |
| luvin | Spindle Output Leakage Current | $\mathrm{V}_{\mathrm{M}}=15 \mathrm{~V}$ |  |  | 100 | $\mu \mathrm{A}$ |
| CURRENT LIMITER |  |  |  |  |  |  |
| $\mathrm{V}_{\text {Lim }}$ | Internal Reference Voltage for current limitation |  | 220 | 240 | 260 | mV |
| $V_{\text {OFFLim }}$ | Comparator Offset |  | -15 |  | +15 | mV |
| THERMAL PROTECTION |  |  |  |  |  |  |
| Ts | Shutdown temperature |  | 130 |  | 170 | ${ }^{\circ} \mathrm{C}$ |
| UNDERVOLTAGE |  |  |  |  |  |  |
| $\mathrm{V}_{\text {ccth (fall) }}$ | Undervoltage threshold (fall) |  | 2.9 | - | - | V |
| $\mathrm{V}_{\text {ccth (rise) }}$ | Undervoltage threshold (rise) |  | - | - | 3.4 | V |
| $\mathrm{V}_{\text {ccth (hys) }}$ | Undervoltage threshold (hys) |  | - | 0.1 | - | V |
| SYSTEM FREQUENCY |  |  |  |  |  |  |
| $\mathrm{f}_{\text {sys }}$ | System frequency | $\begin{aligned} & \hline \mathrm{PRS}=0 \\ & \text { PRS }=1 \end{aligned}$ | $\begin{aligned} & \hline 10 \\ & 20 \end{aligned}$ |  | $\begin{aligned} & 20 \\ & 34 \end{aligned}$ | $\begin{aligned} & \mathrm{MHz} \\ & \mathrm{MHz} \end{aligned}$ |
| SLEW RATE CONTROL |  |  |  |  |  |  |
| $V_{\text {SRC }}$ | SRC Output Voltage |  |  | 1.25 |  | V |
| $\mathrm{I}_{\text {SRC }}$ | Output Current |  |  |  | 500 | $\mu \mathrm{A}$ |
| $\mathrm{R}_{\text {SRC }}$ | External Resistor on pin SRC |  | 10 |  |  | $\mathrm{K} \Omega$ |
| ISR |  |  |  |  |  |  |
| $V_{\text {ISR }}$ | Input Range |  | 0 |  | 2 | V |

Note 1: An SMBJIZAVCL-TR is recommended to clamp $\mathrm{V}_{\mathrm{M}}$ in case of high impedance on power supply line.

## FUNCTIONAL DESCRIPTION

## STB-Thermal protection

Controller drive STB pin by open drain.
When Thermal Shutdown is excited, the device force this pin LOW.
Controller will manage STB to do a re-start.
When STB is LOW all the drivers are shut off.

## Hall Sensor Bias

A regulator on chip supply a $3.3 \mathrm{~V}_{+}-10 \%$ refer-
ence on pin Bias. This regulator can supply an output current up-to 15 mA .
Figure 1.


Figure 2.


Figure 3.


## Inductive Sense Start Up Block

The inductive sense method allows to determine the position and the direction of the starting rotation of the motor.
With the rotor at rest, a voltage Vn is applied subsequently to two motor phases, according to this sequence: UW, VW, VU, WU, WV, UV.
A timer measures the rise time dT to reach the reference current ISR in each phase.
This reference is fixed on the pin ISR with a resistor divider between the pin BIAS and GND.
Through a comparator is possible to determine the phase which has the minimum rise time and so the rotor position is univocally determinated.

Figure 5.


The start up is a procedure allowing to start the motor avoiding any backrotation. This procedure is realized by a customized logic on chip (no modification required in the external microprocessor software).
For the Motor Connection please refer to the Fig. 4.

## Current Limiter

Figure 4. Motor Connections.


The current limiter aim is to avoid that the current in the motor winding overides a fixed threshold value. The voltage input at the pin RF1 is compared with an internal 0.2 V reference.
When the current exceeds the llimit value a flipflop is reset masking (through a combinational logic) the signal to the power windings.

## Rotor Position Detector

This block is connected to the Hall Sensor Output. A comparator with hysteresis receives the sinusoidal hall-sensor signal and generates a squared signal HOUT.
The Zero-Cross signal is generated starting from the HOUT signal as in fig. 5.
The HOUT signal can be read from the microprocessor on the output open drain pin HFG.

## Frequency multiplier

The Frequency Multiplier generates the memory scan frequency (Fscan) starting from the ZeroCross (ZC) signal from the Rotor Position Detector block. The scan frequency relates to the rate of the samples of the input signals.
The number of wave samples in a period $T$ is 36, so this circuit generates 36 pulses between 2 Zero Crossing.

Figure 6.


Fscan has a frequency 36 times of $(1 / T)$. The Fscan is generated from the Zero-cross frequency measured at the previous cycle.
So, if the motor speed changes, the zero-cross is not constant, the Frequency Multiplier adjusts the scan clock, ensuring the synchronization between the Zero-Cross signal and the sinusoidal output voltage.

## Memory and Memory Scan

The memory stores $3 \times 36$ samples describing 3 signals. As each sample is represented in a byte, it may have a value in the range 0 to 255.
The shape of these three signals are designed in order to generate three sinusoidal voltages across the Motor coils ensuring the highest performances in term of power losses and motor speed. The shape of the signals are reported in fig. 7.
In Fig 8 is swown the "differential" voltage across the motor coil U and the motor coil V. Obviously, the voltage shape across the motor coil $U$ and $W$ and the voltage across the motor coil V and W are also sinusoidal and dephased of 120 and 240 degrees respect the voltage shown in fig. 8.
The Memory and Memory scan block receives the scan clock, and at each clock provides the sample addressed by an internal address register.

Figure 7.


Figure 8.


This register is initialized with the memory address of the wave sample synchronized with the Zero-Cross signal. The maximum efficiency (i.e. the maximum motor speed for a particular value of current) for the motor driving may be reached ensuring a particular value PH of dephase between the Zero-Cross signal and the voltage output signal.
This value is written by the external controller using PHS pin (see Phase Shift Block section).

## Kval Block and PWM interface

This unit contains a register storing the Kval value. The Kval value represents a multiplying factor to modulate the 3 profile signals amplitude and it is generated starting from the PWMIN signal coming from the external system controller.
The Kval block receives the PWMIN signals and calculates the Kval value through the reference triangular signal.
This signal is generated by a 10 bit counter that starts counting from 1023 to 0 at Fsys rate, and then restart up to 1023. The resolution is $\pm 1 \mathrm{LSB}$.
Internal triangular wave is synchronized with the PWMIN falling edge.
The PWMIN signal contains information regarding both the amplitude and to the sign of the control variable. If the duty cycle is less than $50 \%$ the Kval is in the range $(-1023,-1)$, while if the duty cycle is equal or greater than $50 \%$ the kval is in the range $(0,1023)$.
A negative Kval value (i.e. PWM duty cycle from 0 to $50 \%$ ) indicates an active brake and generates a 180 degree shift in the voltage profile scan.
The rising edge of the PWMIN signal determines the kval on the reference triangular waveform.
If the PWMIN signal is stable during the entire cycle, the Kval is evaluated according to the following rule:

- PWMIN signal stable to $1->\mathrm{Kval}=+1023$
- PWMIN signal stable to $0->$ Kval $=-1023$

In order to ensure the synchronization between
Figure 9.

the PWMIN signal and the internal signals, the PWMIN signal rate must be calculated by the external microcontroller using the same frequency signal provided to the chip through the pin fsys.

## Digital Multiplier

This unit contains a multiplier executing the multiplication of each sample provided by the memory by the value stored in kval register.
The output value is a 10 -bit word, plus the sign bit.
Figure 10.

## PWM Converter

The PWM converter receives from the digital multiplier three 10 bit digital number and converts it into three PWM signals.
A counter counts up (from 0 to 255) and down (from 255 to 0) at the Fsys rate in continuos mode. Three 8 -bit input registers are written with the 8 most significant bit of the word to be converted and compared to the counter value. The comparator output is:


Figure 11.

-0 , if the input value is smaller than the counter output
-1 , if the input value is equal or greater than the counter output
The comparator output is "adjusted" with a combinational logic with the 2 low significant bit of the word to be converted in order to reach a 10 bit precision.
The comparator output duty cycle is extended with a half fsys period for every low bit step how is showed in the figure 11.

## Phase Shift Block

This block regulates the phase of the driving sig-
nal to control the dephasing between the ZeroCross signal and the voltage sinusoidal output signal.
It is possible to demonstrate that the maximum efficiency for the motor driving may be reached ensuring a particular value PH of dephase between the Zero-Cross signal and the voltage output signal.
The Phase Shift BLock, starting from the PHS input signal synchronize the wave output with the Zero-Cross signal to ensure the optimum dephase.
The PHS signal expresses the phase shift through the duration of its value according to the following rule:

Table 1.

| PHS on | NPhase |  | Phase Shift (degree) |
| :---: | :---: | :---: | :---: |
| time $\mu \mathrm{s}$ (Tsys = 50ns) | decimal | bit |  |
| 0 | 0 | 00000000 | LATCH |
| 0.2 | 1 | 00000001 | 1.25 |
| 0.4 | 2 | 00000010 | 2.50 |
| 0.6 | 3 | 00000011 | 3.75 |
| 0.8 | 4 | 00000100 | 5.00 |
| 1.0 | 5 | 00000101 | 6.25 |
| 1.2 | 6 | 00000110 | 7.50 |
| 1.4 | 7 | 00000111 | 8.75 |
| 1.6 | 8 | 00001000 | 10 |
| 1.8 | 9 | 00001001 | 11.25 |
| 2.0 | 10 | 00001010 | 12.50 |
| 2.2 | 11 | 00001011 | 13.75 |
| 2.4 | 12 | 00001100 | 15.00 |
| 2.6 | 13 | 00001101 | 16.25 |
| 2.8 | 14 | 00001110 | 17.50 |
| 3.0 | 15 | 00001111 | 18.75 |
| 3.2 | 16 | 000010000 | 20 |
| 3.4 | 17 | 000010001 | 21.25 |
| 3.6 | 18 | 000010010 | 22.50 |
| 3.8 | 19 | 000010011 | 23.75 |
| 4.0 | 20 | 000010100 | 25.00 |
| 4.2 | 21 | 000010101 | 26.25 |
| 4.4 | 22 | 000010110 | 27.50 |
| 4.6 | 23 | 000010111 | 28.75 |
|  | . |  | - |
| 16.0 | 80 | 001010000 | 100 |
| 16.2 | 81 | 001010001 | 101.25 |
| 16.4 | 82 | 001010010 | 102.50 |
| 16.6 | 83 | 001010011 | 103.75 |
| 16.8 | 84 | 001010100 | 105.00 |
| 17.0 | 85 | 001010101 | 106.25 |
| 17.2 | 86 | 001010110 | 107.50 |
| 17.4 | 87 | 001010111 | 108.75 |
|  | . | . | . |
|  |  |  |  |
|  | . |  |  |

Table 1. (continued)

| PHS on | NPhase |  | Phase Shift (degree) |
| :---: | :---: | :---: | :---: |
| time $\mu \mathbf{s}$ | decimal | bit |  |
| 56.0 | 280 | 100011000 | 350 |
| 56.2 | 281 | 100011001 | 351.25 |
| 56.4 | 282 | 100011010 | 352.50 |
| 56.6 | 283 | 100011011 | 353.75 |
| 56.8 | 284 | 100011100 | 355.00 |
| 57.0 | 285 | 100011101 | 356.25 |
| 57.2 | 286 | 100011110 | 357.50 |
| 57.4 | 287 | 100011111 | 358.75 |
| $>57.6$ | 288 | 100100000 | 0 |

PHS on = tsys * 4 * Nphase
where: tsys $=50 \mathrm{~ns}$ if fsys $=20 \mathrm{MHz}$
The resulting PHASE SHIFT value is:
PHASE SHIFT = Nphase(8:3) x 10 +

$$
\text { Nphase(2:0) x } 1.25
$$

For istance if Nphase $=00011110$
PHASE SHIFT $=3 \times 10+6 \times 1.25=37.5$

## Low Voltage Detector

This circuit detects if $V_{c c}$ is lower than a fixed threshold. If this event happens the internal logic is resetted and the output FETS are forced in High impedance.

## Slew Rate Control Circuit

This circuit fixes the slew rate for the output stage in order to reduce EMI.
A reference current is generated by means of an internal reference voltage and an external resistor.
The ISRC is used to fix slew rate with a linear law:
Figure 12.


SLEW RATE $=$ RSLR/ISRC $\cdot \frac{\mathrm{V}_{\text {REF }}}{R_{\text {EXT }}}$
$R_{\text {ext }}$ recommended value $>10 \mathrm{~K} \Omega$

## Prescaler Pin

The PRS Pin should be forced to ground when the FSYS frequency is lower (or equal) than 20 MHz and should be forced to Vcc when FSYS frequency is higher than 20 MHz , in order to set the correct timing during the inductive sense, start up and resynchronization phases.
Example of different phase shift settings are shown in the following pictures.

Figure 13. Phase relation between OUTPUT sinusoidal voltage (PWM_IN > 50\%) and Hall sensor signal writin Phase shift $=0^{\circ}$ (default value)


Figure 14. Phase relation between OUTPUT sinusoidal voltage (PWM_IN > 50\%) and Hall sensor signal writing Phase shift $=30^{\circ}$


Figure 15. Phase relation between OUTPUT sinusoidal voltage (PWM_IN > 50\%) and Hall sensor signal writing Phase shift $=330^{\circ}$


| DIM. | mm |  |  | inch |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | MIN. | TYP. | MAX. | MIN. | TYP. | MAX. |
| A | 2.35 |  | 2.65 | 0.093 |  | 0.104 |
| A1 | 0.1 |  | 0.3 | 0.004 |  | 0.012 |
| B | 0.33 |  | 0.51 | 0.013 |  | 0.020 |
| C | 0.23 |  | 0.32 | 0.009 |  | 0.013 |
| D | 12.6 |  | 13 | 0.496 |  | 0.512 |
| E | 7.4 |  | 7.6 | 0.291 |  | 0.299 |
| e |  | 1.27 |  |  | 0.050 |  |
| H | 10 |  | 10.65 | 0.394 |  | 0.419 |
| h | 0.25 |  | 0.75 | 0.010 |  | 0.030 |
| L | 0.4 |  | 1.27 | 0.016 |  | 0.050 |
| K |  |  | $0 \circ(m i n.) 8^{\circ}(m a x)$. |  |  |  |


| OUTLINE AND |
| :---: |
| MECHANICAL DATA |





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