

# 3V to 8V Hot Swap Power Manager

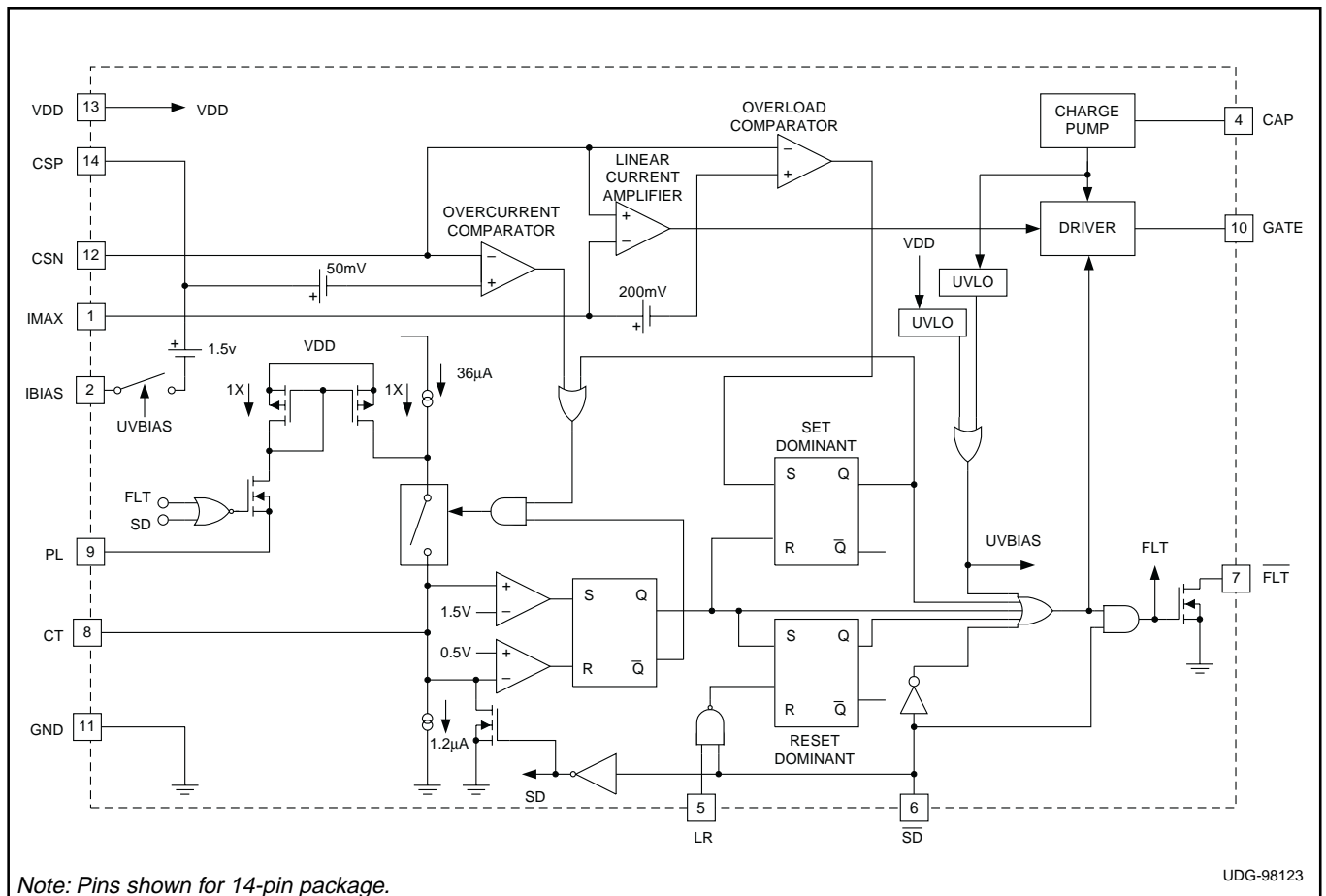
## FEATURES

- Precision Fault Threshold
- Charge Pump for Low RDS<sub>ON</sub> High Side Drive
- Differential Sense Inputs
- Programmable Average Power Limiting
- Programmable Linear Current Control
- Programmable Fault Time
- Fault Output Indicator
- Manual and Automatic Reset Modes
- Shutdown Control w/Programmable Softstart
- Undervoltage Lockout
- Electronic Circuit Breaker Function

## DESCRIPTION

The UCC3919 family of Hot Swap Power Managers provide complete power management, hot swap, and fault handling capability. The UCC3919 features a duty ratio current limiting technique, which provides peak load capability while limiting the average power dissipation of the external pass transistor during fault conditions. The UCC3919 has two reset modes, selected with the TTL/CMOS compatible L/R pin. In one mode, when a fault occurs the IC repeatedly tries to reset itself at a user defined rate, with user defined maximum output current and pass transistor power dissipation. In the other mode the output latches off and stays off until either the L/R pin is reset or the shutdown pin is toggled. The on board charge pump circuit provides the necessary gate voltage for an external N-channel power FET.

## BLOCK DIAGRAM

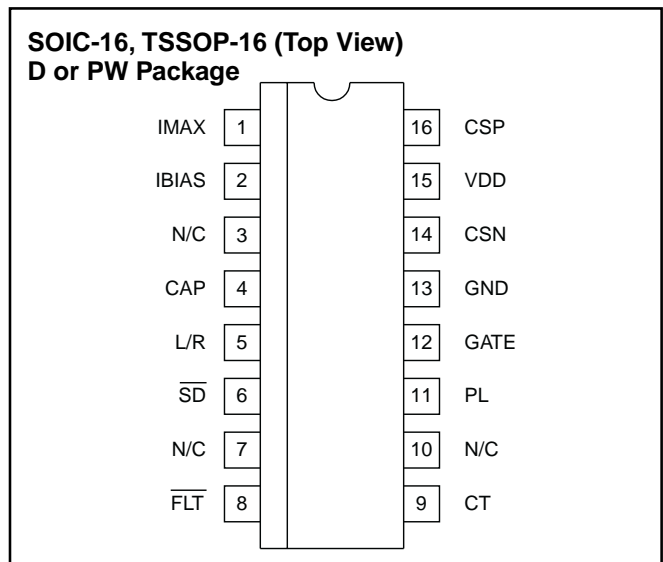
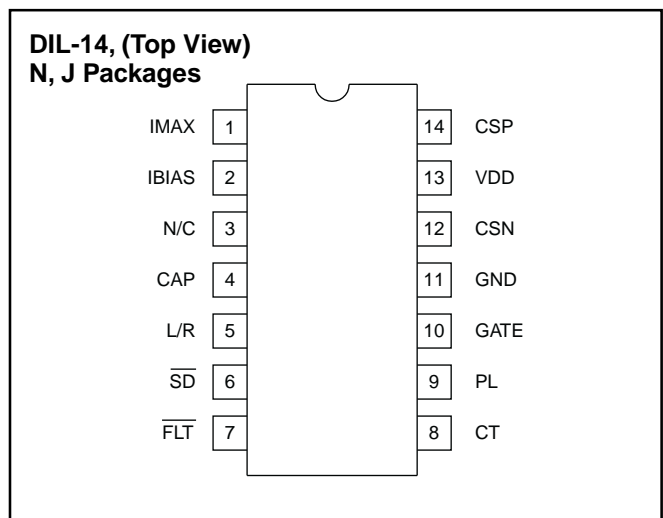


**ABSOLUTE MAXIMUM RATINGS**

VDD . . . . . -0.3V to 10V  
 Pin Voltage  
 (All pins except CAP and GATE) . . . . . -0.3V to VDD + 0.3V  
 Pin Voltage  
 (CAP and GATE) . . . . . -0.3V to 15V  
 PL Current . . . . . 0.5mA to -10mA  
 IBIAS Current . . . . . 0mA to 3mA  
 Storage Temperature . . . . . -65°C to +150°C  
 Junction Temperature . . . . . -55°C to +150°C  
 Lead Temperature (Soldering, 10sec.) . . . . . +300°C

*Currents are positive into, negative out of the specified terminal. Consult Packaging Section of Databook for thermal limitations and considerations of package.*

**CONNECTION DIAGRAMS**



**ELECTRICAL CHARACTERISTICS:** Unless otherwise specified, VDD = 5V, TA = 0°C to 70°C for the UCC3919, -40°C to 85°C for the UCC2919 and -55°C to 125°C for the UCC1919. All voltages are with respect to GND. TA = TJ.

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
<b>Input Supply</b>					
Supply Current	VDD = 3V		0.5	1	mA
	VDD = 8V		1	1.5	mA
Shutdown Current	SD = 0.2V		1	7	µA
<b>Undervoltage Lockout</b>					
Minimum Voltage to Start		2.35	2.75	3	V
Minimum Voltage after Start		1.9	2.25	2.5	V
Hysteresis		0.25	0.5	0.75	V
<b>IBIAS</b>					
Output Voltage, (0µA < IOUT < 15µA)	25°C, referred to CSP	1.47	1.5	1.53	V
	Over Temperature Range, referred to CSP	1.44	1.5	1.56	V
Maximum Output Current		1	2		mA

**ELECTRICAL CHARACTERISTICS:** Unless otherwise specified, VDD = 5V, TA = 0°C to 70°C for the UCC3919, -40°C to 85°C for the UCC2919 and -55°C to 125°C for the UCC1919. All voltages are with respect to GND. TA = TJ.

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
<b>Current Sense</b>					
Over Current Comparator Offset	Referred to CSP, 3V ≤VDD ≤8V	-55	-50	-45	mV
Linear Current Amplifier Offset	V <sub>IMAX</sub> = 100mV, Referred to CSP, 3V ≤VDD ≤8V	-120	-100	-80	mV
	V <sub>IMAX</sub> = 400mV, Referred to CSP, 3V ≤VDD ≤8V	-440	-400	-360	mV
Overload Comparator Offset	V <sub>IMAX</sub> = 100mV, Referred to CSP, 3V ≤VDD ≤8V	-360	-300	-240	mV
CSN Input Common Mode Voltage Range	Referred to VDD, 3V ≤VDD ≤8V, (Note 1)	-1.5		0.2	V
CSP Input Common Mode Voltage Range	Referred to VDD, 3V ≤VDD ≤8V, (Note 1)	0		0.2	V
Input Bias Current CSN			1	5	μA
Input Bias Current CSP			100	200	μA
<b>Current Fault Timer</b>					
CT Charge Current	V <sub>CT</sub> = 1V	-56	-35	-16	μA
CT Discharge Current	V <sub>CT</sub> = 1V	0.5	1.2	1.9	μA
On Time Duty Cycle in Fault	I <sub>PL</sub> = 0	1.5	3	6	%
CT Fault Threshold		1.0	1.5	1.7	V
CT Reset Threshold		0.25	0.5	0.75	V
<b>IMAX</b>					
Input Bias Current	V <sub>IMAX</sub> = 100mV, Referred to CSP	-1	0	1	μA
<b>Power Limiting Section</b>					
Voltage on PL	I <sub>PL</sub> = -250μA, Referred to VDD	-1.0	-1.4	-1.9	V
	I <sub>PL</sub> = -1.5mA, Referred to VDD	-0.5	-1.8	-2.2	V
On Time Duty Cycle in Fault	I <sub>PL</sub> = -250μA	0.25	0.5	1	%
	I <sub>PL</sub> = -1.5mA	0.05	0.1	0.2	%
<b>SD and L/R Inputs</b>					
Input Voltage Low				0.8	V
Input Voltage High		2			V
L/R Input Current		1	3	6	μA
SD Internal Pulldown Impedance		100	270	500	kΩ
<b>FLT Output</b>					
Output Leakage Current	VDD = 5V			10	μA
Output Low Voltage	I <sub>OUT</sub> = 10mA			1	V
<b>FET GATE Driver and Charge Pump</b>					
Peak Output Current	V <sub>CAP</sub> = +15V, V <sub>GATE</sub> = 10V	-3	-1	-0.25	mA
Peak Sink Current	V <sub>GATE</sub> = 5V		20		mA
Fault Delay			100	300	nS
Maximum Output Voltage	VDD = 3V, Average I <sub>OUT</sub> = 1μA	8	10	12	V
	VDD = 8V, Average I <sub>OUT</sub> = 1μA	12	14	16	V
Charge Pump UVLO Minimum Voltage to Start	VDD = 3V	6.5	7.5		V
	VDD = 8V	6.5	8		V
Charge Pump Source Impedance	VDD = 5V, Average I <sub>OUT</sub> = 1μA	50	100	150	kΩ

**Note 1:** Guaranteed by design. Not 100% tested in production.

## PIN DESCRIPTIONS

**CAP:** A capacitor is placed from this pin to ground to filter the output of the on board charge pump. A .01 $\mu$ F to 0.1 $\mu$ F capacitor is recommended .

**CSN:** The negative current sense input signal.

**CSP:** The positive current sense input signal.

**CT:** Input to the duty cycle timer. A capacitor is connected from this pin to ground, setting the off time and the maximum on time of the overcurrent protection circuits.

**FLT:** Fault indicator. This open drain output will pull low under any fault condition where the output driver is disabled. This output is disabled when the IC is in low current standby mode.

**GATE:** The output of the linear current amplifier. This pin drives the gate of an external N-channel MOSFET pass transistor. The linear current amplifier control loop is internally compensated, and guaranteed stable for output load (gate) capacitance between 100pF and .01 $\mu$ F. In applications where the GATE voltage (or charge pump voltage) exceeds the maximum Gate-to-Source voltage ratings ( $V_{GS}$ ) for the external N-channel MOSFET, a Zener clamp may be added to the gate of the MOSFET. No additional series resistance is required since the internal charge pump has a finite output impedance of 100k $\Omega$  typical.

**GND:** The ground reference for the device.

**IBIAS:** Output of the on board bias generator internally regulated to 1.5V below CSP. A resistor divider between this pin and CSP can be used to generate the IMAX voltage. The bias circuit is internally compensated, and requires no bypass capacitance. If an external bypass is required due to a noisy environment, the circuit will be

stable with up to .001 $\mu$ F of capacitance. The bypass must be to CSP, since the bias voltage is generated with respect to CSP. Resistor R2 (Figure 4) should be greater than 50k $\Omega$  to minimize the effect of the finite input impedance of the IBIAS pin on the IMAX threshold.

**IMAX:** Used to program the maximum allowable sourcing current. The voltage on this pin is with respect to CSP. If the voltage across the shunt resistor exceeds this voltage the linear current amplifier lowers the voltage at GATE to limit the output current to this level. If the voltage across the shunt resistor goes more than 200mV beyond this voltage, the gate drive pin GATE is immediately driven low and kept low for one full off time interval.

**L/R:** Latch/Reset. This pin sets the reset mode. If L/R is low and a fault occurs the device will begin duty ratio current limiting. If L/R is high and a fault occurs, GATE will go low and stay low until L/R is set low. This pin is internally pulled low by a 3 $\mu$ A nominal pulldown.

**PL:** Power Limit. This pin is used to control average power dissipation in the external MOSFET. If a resistor is connected from this pin to the source of the external MOSFET, the current in the resistor will be roughly proportional to the voltage across the FET. As the voltage across the FET increases, this current is added to the fault timer charge current, reducing the on time duty cycle from its nominal value of 3% and limiting the average power dissipation in the FET.

**SD:** Shutdown pin. If this pin is taken low, GATE will go low, and the IC will go into a low current standby mode and CT will be discharged. This TTL compatible input must be driven high to turn on.

**VDD:** The power connection for the device.

## APPLICATION INFORMATION

The UCC3919 monitors the voltage drop across a high side sense resistor and compares it against three different voltage thresholds. These are discussed below. Figure 1 shows the UCC3919 waveforms under fault conditions.

### Fault Threshold

The first threshold is fixed at 50mV. If the current is high enough such that the voltage on CSN is 50mV below CSP, the timing capacitor CT begins to charge at about 35 $\mu$ A if the PL pin is open. (Power limiting will be discussed later). If this threshold is exceeded long enough for CT to charge to 1.5V, a fault is declared and the exter-

nal MOSFET will be turned off. It will either be latched off (until the power to the circuit is cycled, the L/R pin is taken low, or the SD pin is toggled), or will retry after a fixed off time (when CT has discharged to 0.5V), depending on whether the L/R pin is set high or low by the user. The equation for this current threshold is simply:

$$I_{FAULT} = \frac{0.05}{R_{SENSE}} \quad (1)$$

The first time a fault occurs, CT is at ground, and must charge 1.5V. Therefore:

$$t_{FAULT} = t_{ON(sec)} = \frac{C_T(\mu F) \cdot 1.5}{35} \quad (2)$$

## APPLICATION INFORMATION

In the retry mode, the timing capacitor will already be charged to 0.5V at the end of the off time, so all subsequent cycles will have a shorter ton time, given by:

$$t_{FAULT} \cong t_{ON}(\text{sec}) = \frac{C_T(\mu F)}{35} \quad (3)$$

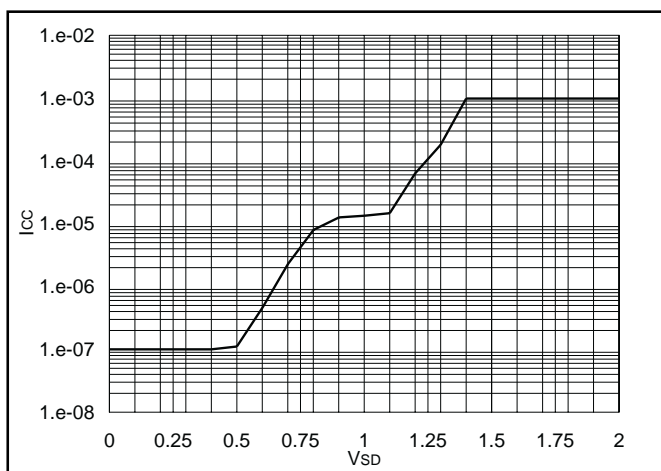
Note that these equations for ton are without the power limiting feature (RPL pin open). The effects of power limiting on ton will be discussed later.

The off time in the retry mode is set by CT and an internal 1.2μA sink current. It is the time it takes CT to discharge from 1.5V to 0.5V. The equation for the off time is therefore:

$$t_{OFF}(\text{sec}) = \frac{C_T \mu F}{1.2} \quad (4)$$

### Shutdown Characteristics

When the  $\overline{SD}$  pin is set to TTL high (above 2V) the UCC3919 is guaranteed to be enabled. When  $\overline{SD}$  is set to a low TTL (below 0.8V) the UCC3919 is guaranteed to be disabled, but may not be in ultra low current sleep mode. When  $\overline{SD}$  is set to 0.2V or less, the UCC3919 is guaranteed to be disabled and in ultra low current sleep mode. See Fig. 1.



**Figure 1. Typical Shutdown Current**

### IMAX Threshold

The second threshold is programmed by the voltage on IMAX (measured with respect to the CSP pin). This controls the maximum current, I<sub>MAX</sub>, that the UCC3919 will allow to flow into the load during the MOSFET on time. A resistive divider connected between IBIAS and CSP generates the programming voltage. When the drop across the sense resistor reaches this voltage, a linear amplifier

reduces the voltage on GATE to control the external MOSFET in a constant current mode.

During this time CT is charging, as described above. If this condition lasts long enough for CT to charge to 1.5V, a fault will be declared and the MOSFET will be turned off. The I<sub>MAX</sub> current is calculated as follows:

$$I_{MAX} = \frac{V_{CSP} - V_{IMAX}}{R_{SENSE}} \quad (5)$$

Note that if the voltage on the IMAX pin is programmed to be less than 50mV below CSP, then the UC3919 will control the MOSFET in a constant current mode all the time. No fault will be declared and the MOSFET will remain on because I<sub>MAX</sub> is less than I<sub>FAULT</sub>.

### Overload Threshold

There is a third threshold which, if exceeded, will declare a fault and shutdown the external MOSFET immediately, without waiting for CT to charge. This “Overload” threshold is 200mV greater than the IMAX threshold (again, this is with respect to CSP). This feature protects the circuit in the event that the external MOSFET is on, with a load current below I<sub>MAX</sub>, and a short is quickly applied across the output. This allows hot-swapping in cases where the UCC3919 is already powered up (on the backplane) and capacitors are added across the output bus. In this case, the load current could rise too quickly for the linear amplifier to reduce the voltage on GATE and limit the current to I<sub>MAX</sub>. If the overload threshold is reached, the MOSFET will be turned off quickly and a fault declared. A latch is set so that CT can be charged, guaranteeing that the MOSFET will remain off for the same period as defined above before retrying. The overload current is:

$$I_{OVERLOAD} = \frac{V_{CSP} - V_{IMAX} + 0.2}{R_{SENSE}} = I_{MAX} + \frac{0.2}{R_{SENSE}} \quad (6)$$

Note that I<sub>OVERLOAD</sub> may be much greater than I<sub>MAX</sub>, depending on the value of R<sub>SENSE</sub>.

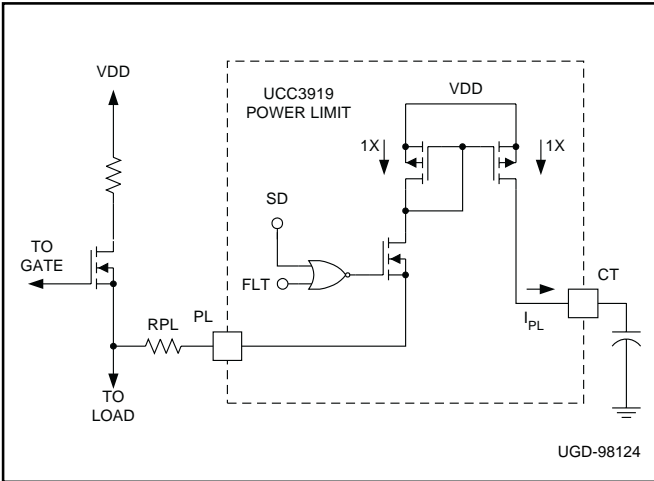
### Power Limiting

A power limiting feature is included which allows the power dissipated in the external MOSFET to be held relatively constant during a short, for different values of input voltage. This is accomplished by connecting a resistor from the output (source of the external MOSFET) to PL. When the output voltage drops due to a short or overload, an internal bias current is generated which is equal to:

$$I_{PL} \cong \frac{(V_{IN} - V_{OUT} - V_{PL})}{R_{PL}} \quad (7)$$

**APPLICATION INFORMATION (cont.)**

This current is used to help charge the timing capacitor in the event that the load current exceeds  $I_{FAULT}$ . (A simplified schematic of the circuit internal to the UCC3919 is shown in Figure 2.) The result is that the on time of the MOSFET during current limit is reduced as the input voltage is increased. This reduces the effective duty cycle, holding the average power dissipated constant.



**Figure 2. Power limiting circuit.**

It can be seen that power limiting will only occur when  $I_{PL}$  is  $> 0$  (it cannot be negative). For power limiting to begin to occur, the voltage drop across the MOSFET must be greater than  $V_{DD} - V_{PL}$  or 1.4V(typ).

$$V_{IN} - V_{OUT} \geq 1.4V \quad (8)$$

The on time using  $R_{PL}$  is defined as:

$$t_{ON} = \frac{C_T \cdot \Delta V}{I_{PL} + 35 \cdot 10^{-6}} \quad \text{where } \Delta V = 1V \quad (9)$$

The graph in Figure 4 illustrates the effect of  $R_{PL}$  on the average MOSFET power dissipation into a short. The equation for the average power dissipation during a short is:

$$P_{DISS} = \frac{I_{MAX} \cdot V_{IN} \cdot 1.2 \cdot 10^{-6}}{I_{PL} + 35 \cdot 10^{-6}}, \text{ or} \quad (10)$$

$$P_{DISS} = \frac{I_{MAX} \cdot V_{IN} \cdot t_{ON}}{t_{ON} + t_{OFF}}$$

If  $PL$  is left unconnected, the power limiting feature will not be exercised. In the retry mode, the duty cycle during a fault will be nominally 3%, independent of input voltage. The average power dissipation in the external MOSFET with a shorted output will be proportional to input voltage, as shown by the equation:

$$P_{DISS} = I_{MAX} \cdot V_{IN} \cdot 0.033 \quad (11)$$

**Calculating  $C_T(\min)$  for a Given Load Capacitance without Power Limiting**

To guarantee recovery from an overload when operating in the retry mode, there is a maximum total output capacitance which can be charged for a given  $t_{ON}$  (fault time) before causing a fault. For a worst case situation of a constant current load below the fault threshold,  $C_T(\min)$  for a given output load capacitance (without power limiting) can be calculated from:

$$C_T(\min) = \frac{V_{IN} \cdot C_{OUT} \cdot 35 \cdot 10^{-6}}{I_{MAX} - I_{LOAD}} \quad (12)$$

A larger load capacitance or a smaller  $C_T$  will cause a fault when recovering from an overload, causing the circuit to get stuck in a continuous hiccup mode. To handle larger capacitive loads, increase the value of  $C_T$ . The equation can be easily re-written, if desired, to solve for  $C_{OUT(max)}$  for a given value of  $C_T$ .

For a resistive load of value  $R_L$  and an output cap  $C_{OUT}$ ,  $C_T(\min)$  can be smaller than in the constant current case, and can be estimated from:

$$C_T(\min) = \frac{-C_{OUT} \cdot R_L \cdot \ln\left(1 - \frac{V_{IN}}{I_{MAX} \cdot R_L}\right)}{28 \cdot 10^3} \quad (13)$$

Note that in the latch mode (or when first turning on in the retry mode), since the timing capacitor is not recovering from a previous fault, it is charging from 0V rather than 0.5V. This allows up to 50% more load capacitance without causing a fault.

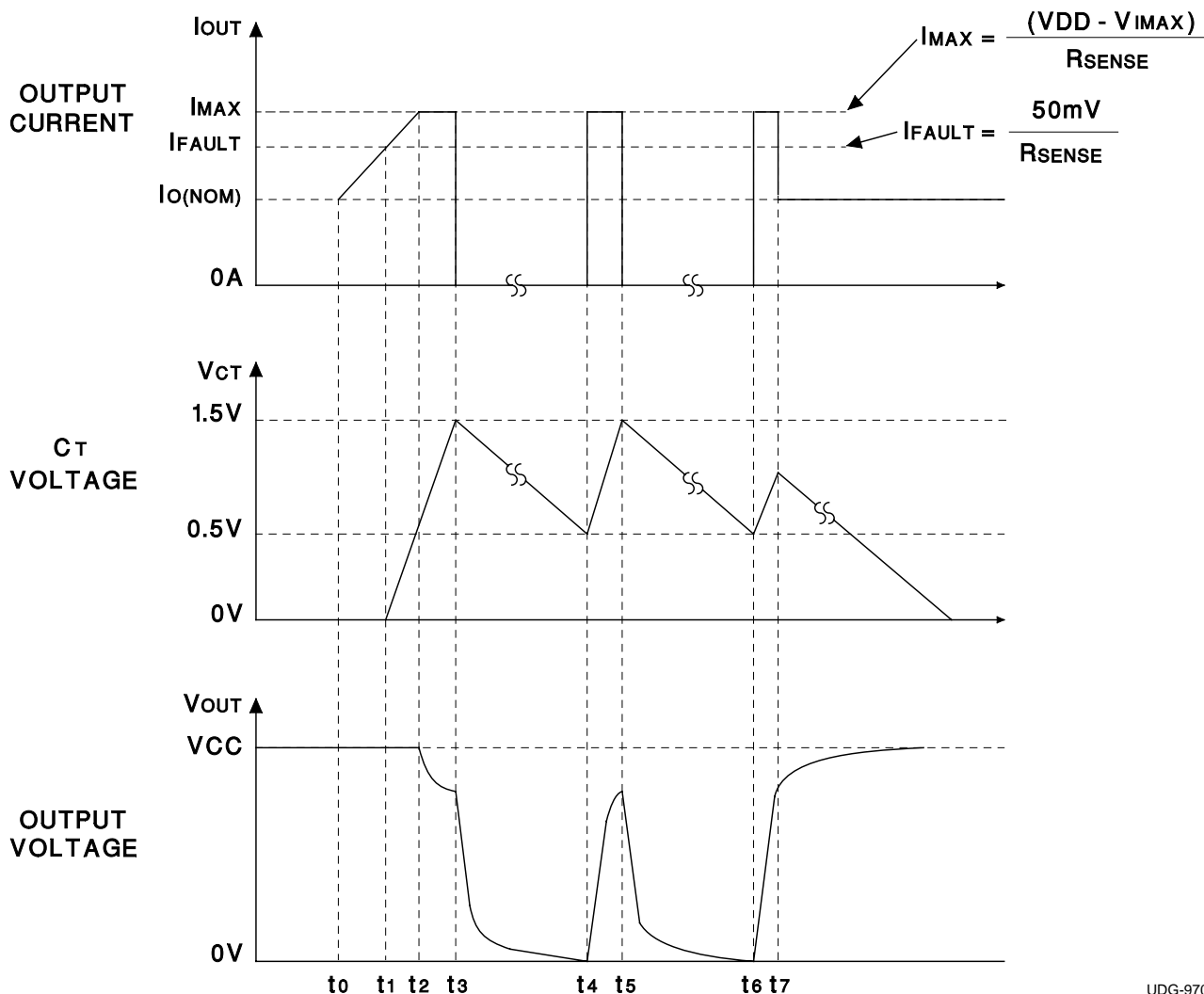
**Estimating  $C_T(\min)$  When Using Power Limiting**

If power limiting is used, the calculation of  $C_T(\min)$  for a given  $C_{OUT}$  becomes considerably more complex, especially with a resistive load. This is because the  $C_T$  charge current becomes a function of  $V_{OUT}$ , which is changing with time. The amount of capacitance that can be charged (without causing a fault) when using power limiting will be significantly reduced for the same value  $C_T$ , due to the shorter  $t_{on}$  time.

The charge current contribution from the power limiting circuit is defined as:

$$I_{PL} \cong \frac{(V_{IN} - V_{OUT} - V_{PL})}{R_{PL}} \quad (14)$$

APPLICATION INFORMATION (cont.)



UDG-97073

**t0:** Normal condition - Output current is nominal, output voltage is at positive rail,  $V_{CC}$ .

**t1:** Fault control reached - Output current rises above the programmed fault value,  $C_T$  begins to charge with  $35\mu A + I_{PL}$ .

**t2:** Maximum current reached - Output current reaches the programmed maximum level and becomes a constant current with value  $I_{MAX}$ .

**t3:** Fault occurs -  $C_T$  has charged to 1.5V, fault output

goes low, the FET turns off allowing no output current to flow,  $V_{OUT}$  discharges to GND.

**t4:** Retry -  $C_T$  has discharged to 0.5V, but fault current is still exceeded,  $C_T$  begins charging again, FET is on,  $V_{OUT}$  increases.

**t3 to t5:** Illustrates <3% duty cycle depending upon RPL selected.

**t6 = t4**

**t7:** Fault released, normal condition - return to normal operation of the circuit breaker

Figure 3. Typical Timing Diagram

### APPLICATION INFORMATION (cont.)

#### Constant Current Load

For a constant current load, the output capacitor will charge linearly. During that time:

$$I_{PL} (avg) \cong \frac{(V_{IN} - V_{PL})^2}{2 \cdot R_{PL} \cdot V_{IN}} \quad (15)$$

Modifying equation (12) yields:

$$C_T (min) \cong \frac{V_{IN} \cdot C_{OUT} \cdot \left[ \frac{(V_{IN} - V_{PL})^2}{2 \cdot R_{PL} \cdot V_{IN}} + 35 \cdot 10^{-6} \right]}{I_{MAX} - I_{LOAD}} \quad (16)$$

#### Resistive Load

Determining  $C_T(min)$  for a resistive load is more complex. First, the expression for the output voltage as a function of time is:

$$V_{OUT}(t) = I_{MAX} \cdot R_{LOAD} \left( 1 - e^{-\frac{T_{START}}{R_{LOAD} \cdot C_{OUT}}} \right) \quad (17)$$

Solving for  $T_{START}$  when  $V_{OUT} = V_{IN}$  yields:

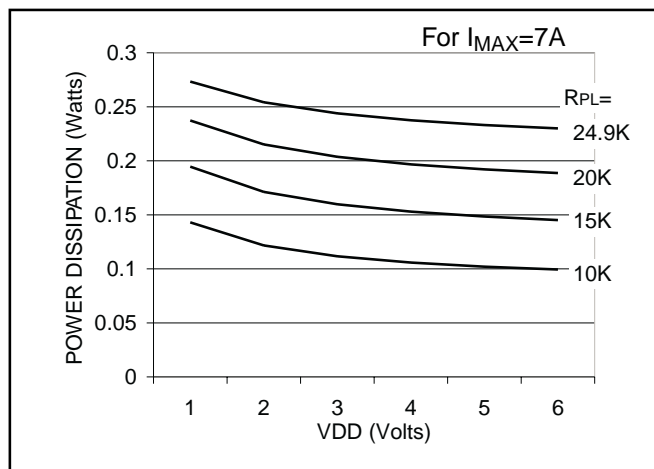


Figure 4. MOSFET average short circuit power dissipation vs.  $V_{IN}$  for values of  $R_{PL}$ .

$$T_{START} = -R_{LOAD} \cdot C_{OUT} \cdot \ln \left( 1 - \left( \frac{V_{IN}}{I_{MAX} \cdot R_{LOAD}} \right) \right) \quad (18)$$

Assuming that the device is operating in the retry mode, where  $C_T$  is charging from 0.5V to just below 1.5V in time  $t$ ,  $C_T$  is defined as:

$$C_T = \frac{I_{CT} \cdot dt}{dV} = I_{CT} \cdot dt \quad \text{Where} \quad (19)$$

$$I_{CT} = (I_{PL} + 35 \cdot 10^{-6})$$

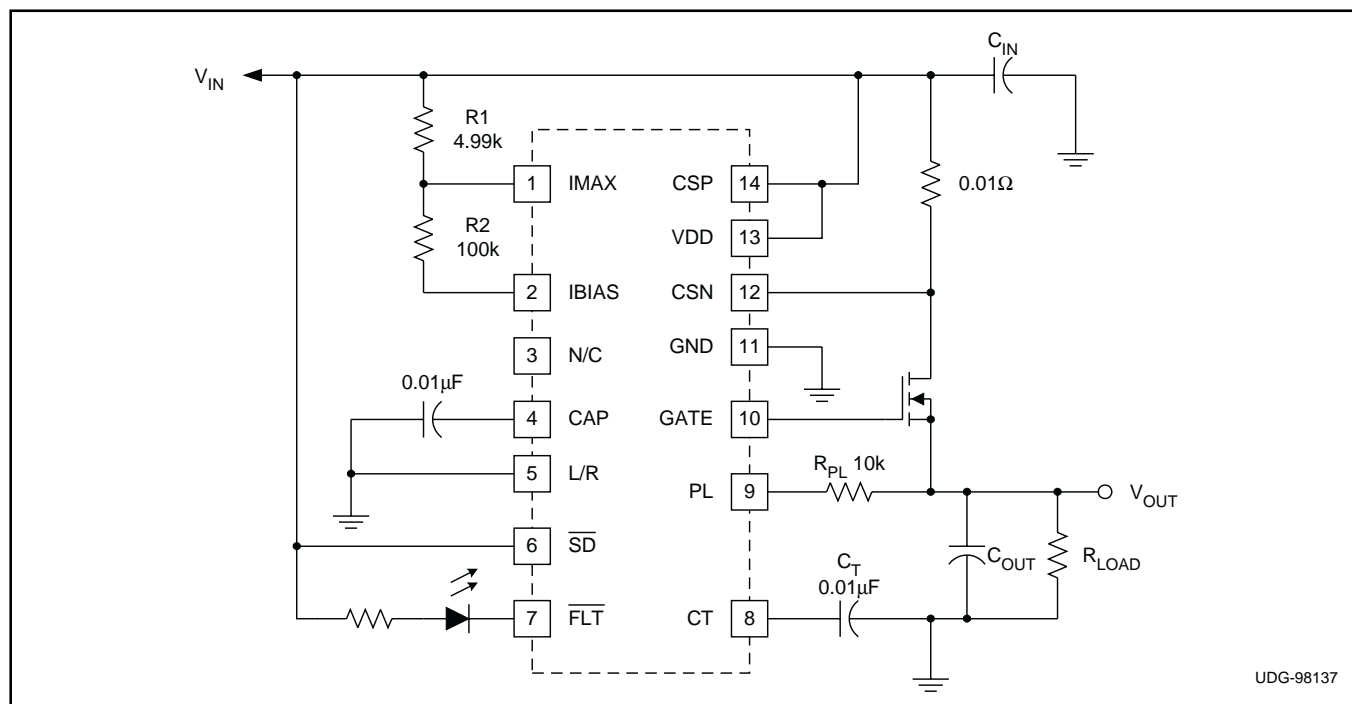


Figure 5. Application circuit.



**APPLICATION INFORMATION (cont.)**

Substituting equation (15) into (19) yields:

$$C_T(\text{min}) = \left( \frac{(V_{IN} - V_{PL})^2}{2 \cdot R_{PL} \cdot V_{IN}} + 35 \cdot 10^{-6} \right) \cdot dt \quad (20)$$

This yields the following expression for  $C_T(\text{min})$  for a resistive load with power limiting. By substituting the value calculated for  $T_{START}$  in equation (18) for  $dt$ ,  $C_T(\text{min})$  is determined.

$$C_T(\text{min}) = \left[ \frac{(V_{IN} \cdot V_{PL})^2}{2 \cdot R_{PL} \cdot V_{IN}} + 35 \cdot 10^{-6} \right] \cdot T_{START} \quad (21)$$

**Example**

The example in Figure 5 shows the UCC3919 in a typical application. A low value sense resistor and N-channel MOSFET minimize losses. With the values shown for R1, R2, and Rs, the overcurrent fault will be 5A nominal. Linear current limiting ( $I_{MAX}$ ) will occur at 7.14A and the overload comparator will trip at 27A. The calculations are shown below.

$$I_{FAULT} = \frac{0.05}{R_S} = \frac{0.05}{0.01} = 5A \quad (22)$$

$$I_{MAX} = \frac{V_{CSP} - V_{IMAX}}{R_S} = \frac{1.5 \cdot R1}{(R1 + R2) \cdot R_S} = 7.14A \quad (23)$$

$$I_{OVERLOAD} = I_{MAX} + \frac{0.2}{R_S} = 7.14A + \frac{0.2}{0.01} = 27.14A \quad (24)$$

$$T_{OFF}(\text{sec}) = \frac{C_T \mu F}{1.2} = \frac{0.01}{1.2} = 8.33 \text{ ms} \quad (25)$$

With the value shown for  $R_{PL}$ :

$$I_{PL(\text{typ})}(\text{output shorted}) = \left( \frac{V_{IN} - V_{PL}}{R_{PL}} \right) = \left( \frac{5 - 1.6}{10K} \right) = 340 \mu A \quad (26)$$

$$t_{ON}(\text{shorted}) = \frac{C_T}{I_{PL} + 35 \cdot 10^{-6}} = \frac{0.01 \cdot 10^{-6}}{375 \mu A} = 27 \mu s \quad (27)$$

$$P_{DISS}(\text{shorted}) = \frac{I_{MAX} \cdot V_{IN} \cdot t_{ON}}{t_{ON} + t_{OFF}} \quad (28)$$

$$= \frac{7.14 \cdot 5 \cdot 27 \mu s}{27 \mu s + 8.33 \cdot 10^{-3}} = 0.12W$$

For a worst case 1Ω resistive load:  $C_{OUT}(\text{max}) \cong 47 \mu F$ .

For a worst case 5A constant current load:  $C_{OUT}(\text{max}) \cong 27 \mu F$ .

With L/R grounded, the part will operate in the retry or “hiccup” mode. The values shown for  $C_T$  and  $R_{PL}$  will yield a nominal duty cycle of 0.32% and an off time of 8.3ms. With a shorted output, the average steady state power dissipation in Q1 will be less than 100mW over the full input voltage range.

If power limiting is disabled by opening  $R_{PL}$ , then:

$$t_{FAULT} = t_{ON} \text{ sec} = \frac{C_T \mu F \cdot 1}{35} = 287 \mu s \quad (29)$$

$$P_{DISS}(\text{shorted}) = \frac{I_{MAX} \cdot V_{IN} \cdot t_{ON}}{t_{OFF} + t_{ON}} \quad (30)$$

$$= \frac{7.14 \cdot 5 \cdot 287 \cdot 10^{-6}}{287 \cdot 10^{-6} + 8.33 \cdot 10^{-3}} = 1.2W \text{ (with } V_{IN} = 5V)$$

For a worst case 1Ω resistive load:  $C_{OUT}(\text{max}) \cong 220 \mu F$ .

For a worst case 5A constant current load:  $C_{OUT}(\text{max}) \cong 120 \mu F$ .

**THERMAL CONSIDERATIONS**

**Steady State Conditions**

In normal operation, with a steady state load current below  $I_{FAULT}$ , the power dissipation in the external MOSFET will be:

$$P_{DISS} = R_{DS\ ON} \cdot I_{LOAD}^2 \quad (31)$$

The junction temperature of the MOSFET can be calculated from:

$$T_J = T_A + (P_{DISS} \cdot \theta_{JA}) \quad (32)$$

Where  $T_A$  is the ambient temperature and  $\theta_{JA}$  is the MOSFET's thermal resistance from junction to ambient. If the device is on a heatsink, then the following equation:

$$\theta_{JA} + \theta_{JC} + \theta_{CS} + \theta_{SA} \quad (33)$$

Where  $\theta_{JC}$  is the MOSFET's thermal resistance from junction to case,  $\theta_{CS}$  is the thermal resistance from case to sink, and  $\theta_{SA}$  is the thermal resistance of the heatsink to ambient.

The calculated  $T_J$  must be lower than the MOSFET's maximum junction temperature rating, therefore:

$$\theta_{JA} < \frac{T_J(\text{max}) - T_A}{P_{DISS}} \quad (34)$$

## APPLICATION INFORMATION

### Transient Thermal Impedance

During a fault condition in the retry mode, the average MOSFET power dissipation will generally be quite low due to the low duty cycle, as defined by:

$$P_{DISS}(avg) = \frac{I_{MAX} \cdot V_{IN} \cdot t_{ON}}{t_{ON} + t_{OFF}} \quad (\text{w/output shorted}) \quad (35)$$

(In the latch mode,  $t_{OFF}$  will be the time between a fault and the time the device is reset.)

However, the pulse power in the MOSFET during  $t_{ON}$ , with the output shorted, is:

$$P_{DISS}(pulse) = I_{MAX} \cdot V_{IN} \quad (\text{w/output shorted}) \quad (36)$$

In choosing  $t_{ON}$  for a given  $V_{IN}$ ,  $I_{MAX}$ , and duty cycle it is important to consult the manufacturer's transient thermal impedance curves for the MOSFET to make sure the device is within its safe operating area. These curves provide the user with the effective thermal impedance of the device for a given time duration pulse and duty cycle. Note that some of the impedance curves are normalized to one, in which case the transient impedance values must be multiplied by the DC (steady state) thermal resistance,  $\theta_{JC}$ .

For duty cycles not shown in the manufacturer's curves, the transient thermal impedance for any duty cycle and ton time (given a square pulse) can be estimated from [1]:

$$\theta_{JC}(trans) = (D \cdot \theta_{JC}) + (1 - D) \cdot \theta_{SP} \quad (37)$$

where D is the duty cycle:  $\frac{t_{ON}}{t_{ON} + t_{OFF}}$ .

and  $\theta_{SP}$  is the single pulse thermal impedance given in the transient thermal impedance curves for the time duration of interest ( $t_{ON}$ ). Note that these are absolute numbers, not normalized. If the given single pulse impedance is normalized, it must first be multiplied by  $\theta_{JC}$  before using in the equation above.

This effective transient thermal impedance, when multiplied by the pulse power, will give the transient temperature rise of the die. To keep the junction temperature below the maximum rating, the following must be true:

$$\theta_{JC}(trans) = \frac{T_J(max) - T_C}{P_{DISS}(pulse)} \quad (38)$$

If necessary, the junction temperature rise can be reduced by reducing  $t_{ON}$  (using a smaller value for  $C_T$ ), or by reducing the duty cycle using the power limiting feature already discussed. Note that in either case, the amount of load capacitance,  $C_{OUT}$ , that can be charged before causing a fault, will also be reduced.

### Safety Recommendations

Although the UCC3919 is designed to provide system protection for all fault conditions, all integrated circuits can ultimately fail short. For this reason, if the UCC3919 is intended for use in safety critical applications where UL or some other safety rating is required, a redundant safety device such as a fuse should be placed in series with the device. The UCC3919 will prevent the fuse from blowing for virtually all fault conditions, increasing system reliability and reducing maintenance cost, in addition to providing the hot swap benefits of the device.

### References

- [1] International Rectifier, HEXFET Power MOSFET Designer's Manual, Application Note 949B, *Current Ratings, Safe Operating Area, and High Frequency Switching Performance of Power HEXFETs*, pp.1553-1565, September 1993.

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