UNITRODE

High Performance Power Factor Preregulator

FEATURES

- Controls Boost PWM to Near Unity Power Factor

- Fixed Frequency Average Current Mode Control Minimizes Line Current Distortion

- Built-in Active Snubber (ZVT) allows Operation to 500kHz, improved EMI and Efficiency

- Inductor Current Synthesizer allows Single Current Transformer Current Sense for Improved Efficiency and Noise Margin

- Accurate Analog Multiplier with Line Compensator allows for Universal Input Voltage Operation

- High Bandwidth (5MHz), Low Offset Current Amplifier

- Overvoltage and Overcurrent protection

- Two UVLO Threshold Options

- 150μA Startup Supply Current Typical
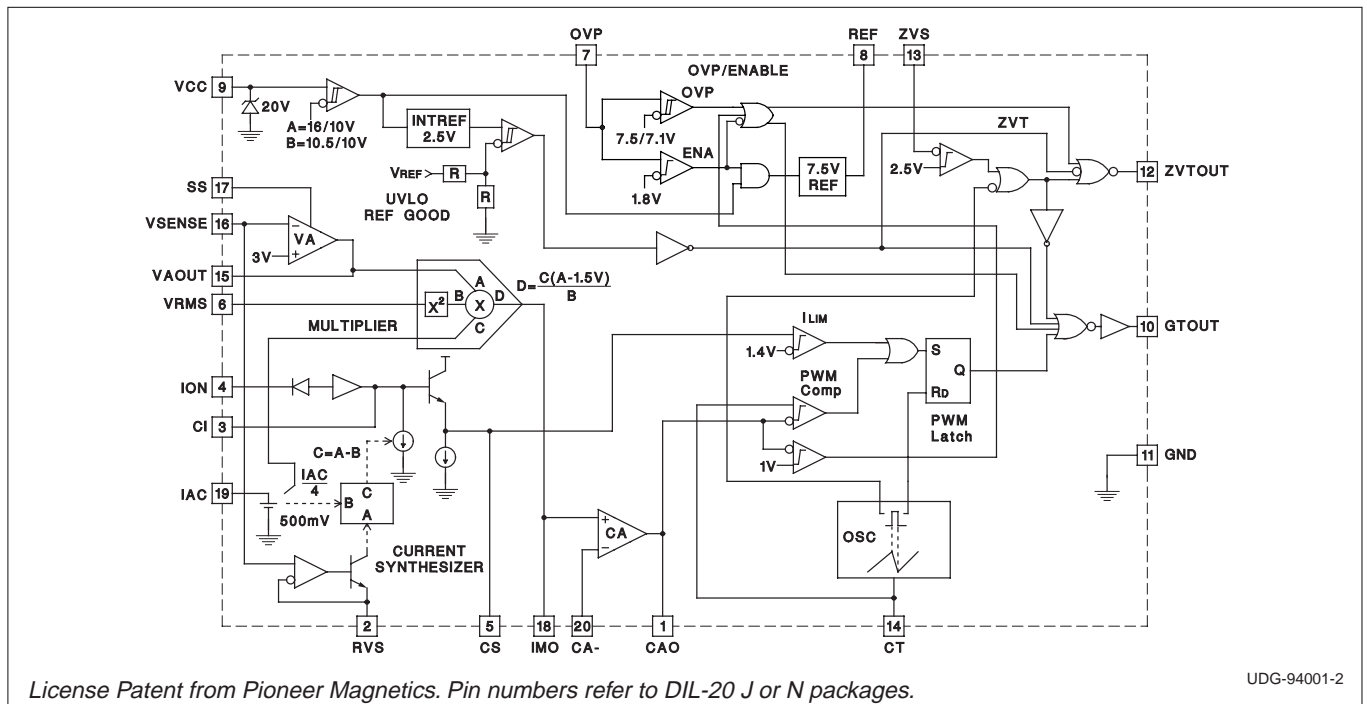
- Precision 1% 7.5V Reference

DESCRIPTION

The UC1855A/B provides all the control features necessary for high power, high frequency PFC boost converters. The average current mode control method allows for stable, low distortion AC line current programming without the need for slope compensation. In addition, the UC1855 utilizes an active snubbing or ZVT (Zero Voltage Transition technique) to dramatically reduce diode recovery and MOSFET turn-on losses, resulting in lower EMI emissions and higher efficiency. Boost converter switching frequencies up to 500kHz are now realizable, requiring only an additional small MOSFET, diode, and inductor to resonantly soft switch the boost diode and switch. Average current sensing can be employed using a simple resistive shunt or a current sense transformer. Using the current sense transformer method, the internal current synthesizer circuit buffers the inductor current during the switch on-time, and reconstructs the inductor current during the switch off-time. Improved signal to noise ratio and negligible current sensing losses make this an attractive solution for higher power applications.

The UC1855A/B also features a single quadrant multiplier, squarer, and divider circuit which provides the programming signal for the current loop. The internal multiplier current limit reduces output power during low line conditions. An overvoltage protection circuit disables both controller outputs in the event of a boost output OV condition.

Low startup supply current, UVLO with hysteresis, a 1% 7.5V reference, voltage amplifier with softstart, input supply voltage clamp, enable comparator, and overcurrent comparator complete the list of features. Available packages include: 20 pin N, DW, Q, J, and L.
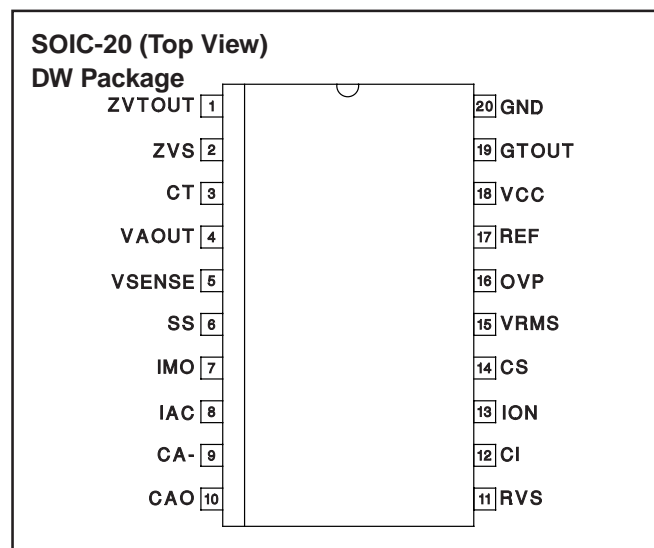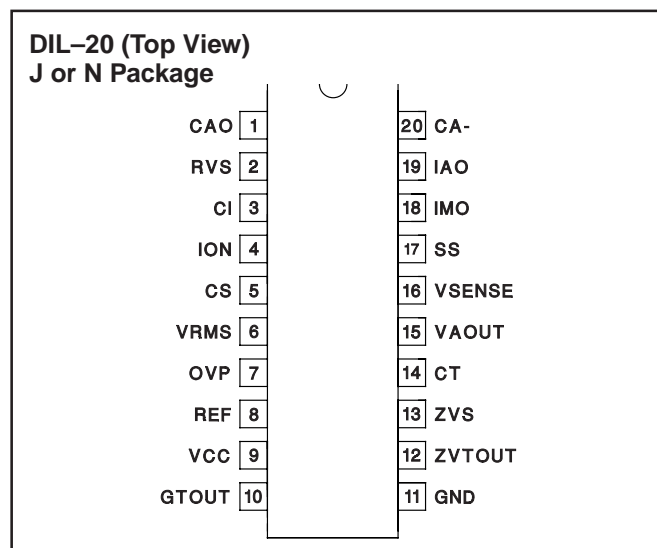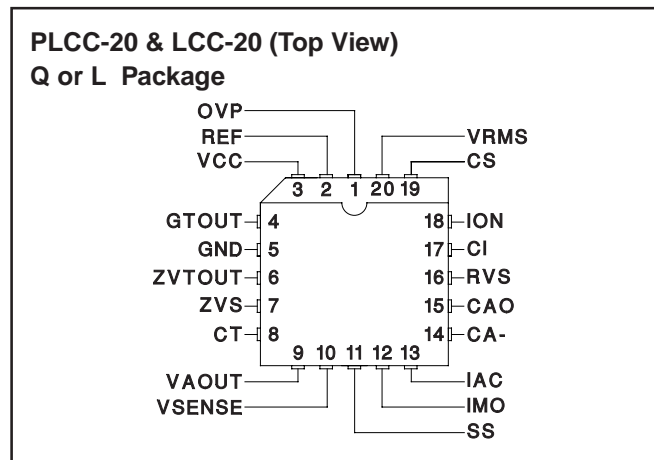
BLOCK DIAGRAM

License Patent from Pioneer Magnetics. Pin numbers refer to DIL-20 J or N packages.

UDG-94001-2

ABSOLUTE MAXIMUM RATINGS

Supply Voltage VCC. . . . . Internally Limited
VCC Supply Clamp Current 20mA
PFC Gate Driver Current (continuous) . . . . ± 0.5A
PFC Gate Driver Current (peak) . . . . ± 1.5A
ZVT Drive Current (continuous) . . . . ± 0.25A
ZVT Drive Current (peak) . . . . ± 0.75A
Input Current (IAC, R_T, RVA) 5mA
Analog Inputs (except Peak Limit). . . . . –0.3 to 10V
Peak Limit Input . . . . –0.3 to 6.5V
Softstart Sinking Current 1.5mA
Storage Temperature . . . . –65°C to +150°C
Junction Temperature. . . . . –55°C to +150°C
Lead Temperature (Soldering, 10 sec.) . . . . +300°C

Currents are positive into, negative out of the specified terminal. Consult Packaging Section of Databook for thermal limitations and considerations of packages. All voltages are referenced to GND.

CONNECTION DIAGRAMS

PLCC-20 & LCC-20 (Top View)
Q or L Package

DIL–20 (Top View)
J or N Package

SOIC-20 (Top View)
DW Package

ELECTRICAL CHARACTERISTICS:

Unless otherwise specified: VCC = 18V, R_T = 15k, RVS = 23k, CT = 470pF, CI = 150pF, VRMS = 1.5V, IAC = 100μA, I_{SENSE} = 0V, CA_{OUT} = 4V, VAOUT= 3.5V, VSENSE = 3V. T_A = T_J. T_A = –55°C to 125°C (UC1855A/B), –40°C to 85°C (UC2855A/B), 0°C to 70°C (UC3855A/B).

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
Overall					
Supply Current, OFF	CAO, VAOUT = 0V, VCC = UVLO –0.3V		150	500	μA
Supply Current, OPERATING			17	25	mA
VCC Turn-On Threshold	UC1855A		15.5	17.5	V
VCCTurn-Off Threshold	UC1855A,B	9	10		V
VCC Turn-On Threshold	UC1855B		10.5	10.8	V
VCC Clamp	I(VCC) = $I_{CC(on)}$ + 5mA	18	20	22	V
Voltage Amplifier					
Input Voltage		2.9		3.1	V
VSENSE Bias Current		–500	25	500	nA
Open Loop Gain	V_{OUT} = 2 to 5V	65	80		dB
V_{OUT} High	I_{LOAD} = –300μA	5.75	6	6.25	V
V_{OUT} Low	I_{LOAD} = 300μA		0.3	0.5	V
Output Short Circuit Current	V_{OUT} = 0V		0.6	3	mA

ELECTRICAL CHARACTERISTICS: Unless otherwise specified: VCC = 18V, R_T = 15k, RVS = 23k, CT = 470pF, CI = 150pF, VRMS = 1.5V, IAC = 100μA, I_{SENSE} = 0V, CA_{OUT} = 4V, VAOUT= 3.5V, VSENSE = 3V. T_A = T_J. T_A = –55°C to 125°C (UC1855A/B), –40°C to 85°C (UC2855A/B), 0°C to 70°C (UC3855A/B).

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
Current Amplifier					
Input Offset Voltage	V_{CM} = – 2.5V	–4		4	mV
Input Bias Current (Sense)	V_{CM} = 2.5V	–500		500	nA
Open Loop Gain	V_{CM} = 2.5V, V_{OUT} = 2 to 6V	80	110		dB
V_{OUT} High	I_{LOAD} = –500μA		6		V
V_{OUT} Low	I_{LOAD} = 500μA		0.3	0.5	V
Output Short Circuit Current	V_{OUT} = 0V		1	3	mA
Common Mode Range		–0.3		5	V
Gain Bandwidth Product	F_{IN} = 100kHz, 10mV, P–P, T_A = 25°C	2.5	5		MHz
Reference					
Output Voltage	I_{REF} = 0mA, T_A = 25°C	7.388	7.5	7.613	V
	I_{REF} = 0mA	7.313	7.5	7.688	V
Load Regulation	I_{REF} = 1 to 10 mA	–15		15	mV
Line Regulation	VCC = 15 to 35V	–10		10	mV
Short Circuit Current	REF = 0V	20	45	65	mA
Oscillator					
Initial Accuracy	T_A = 25°C	170	200	230	kHz
Voltage Stability	V_{CC} = 12 to 18V		1		%
Total Variation	Line, Temp.	160		240	kHz
Ramp Amplitude (P–P)		4.9		5.9	V
Ramp Valley Voltage		1.1		1.6	V
Enable/OVP/Current Limit					
Enable Threshold			1.8	2.2	V
OVP Threshold			7.5	7.66	V
OVP Hysteresis		200	400	600	mV
OVP Propagation Delay			200		ns
OVP Input Bias Current	V= 7.5V		1	10	μA
PK_{LIMIT} Threshold		1.25	1.5	1.75	V
PK_{LIMIT} Input Current	$V_{PKLIMIT}$ = 1.5V		100		μA
PK_{LIMIT} Prop. Delay			100		ns
Multiplier					
Output Current - IAC Limited	IAC = 100μA, VRMS = 1V	–235	–205	–175	μA
Output Current - Zero	IAC = 0μA	–2	–0.2	2	μA
Output Current - Power Limited	VRMS = 1.5V, VAOUT = 5.5V	–250	–209	–160	μA
Output Current	VRMS = 1.5V, VAOUT = 2V		–26		μA
	VRMS = 1.5V VAOUT = 5V		–190		μA
	VRMS = 5V, VAOUT = 2V		–3		μA
	VRMS = 5V, VAOUT = 5V		–17		μA
Gain Constant	Refer to Note 1	–0.95	–0.85	–0.75	1/V
Gate Driver Output					
Output High Voltage	I_{OUT} = –200mA, VCC = 15V	12	12.8		V
Output Low Voltage	I_{OUT} = 200mA		1	2.2	V
Output Low Voltage	I_{OUT} = 10mA		300	500	mV
Output Low (UVLO)	I_{OUT} = 50mA, VCC = 0V		0.9	1.5	V
Output RISE/FALL Time	C_{LOAD} = 1nF		35		ns
Output Peak Current	C_{LOAD} = 10nF		1.5		A

ELECTRICAL CHARACTERISTICS: Unless otherwise specified: VCC = 18V, R_T = 15k, RVS = 23k, CT = 470pF, CI = 150pF, VRMS = 1.5V, IAC = 100µA, I_{SENSE} = 0V, CA_{OUT} = 4V, VAOUT= 3.5V, VSENSE = 3V. T_A = T_J. T_A = −55°C to 125°C (UC1855A/B), −40°C to 85°C (UC2855A/B), 0°C to 70°C (UC3855A/B).

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
ZVT					
Reset Threshold		2.3	2.6	2.9	V
Input Bias Current	V = 2.5V, V_{CT} = 0		6	20	µA
Propagation Delay	Measured at ZVTOUT		100		ns
Maximum Pulse Width			400		ns
Output High Voltage	I_{OUT} = −100mA, V_{CC} = 15V	12	12.8		V
Output Low Voltage	I_{OUT} = 100mA		1	2.2	V
	I_{OUT} = 10mA		300	900	mV
Output Low (UVLO)	I_{OUT} = 50mA, V_{CC} = 0V		0.9	1.5	V
Output RISE/FALL Time	C_{LOAD} = 1nF		35		ns
Output Peak Current	C_{LOAD} = 10nF		0.75		A
Current Synthesizer					
I_{ON} to CS Offset	VION = 0V		30	50	mV
CI Discharge Current	IAC = 50µA	105	118	140	µA
	IAC = 500µA		5		µA
IAC Offset Voltage		0.3	0.65	1.1	V
ION Buffer Slew Rate			10		V/µs
ION Input Bias Current	V_{ION} = 2V		2	15	µA
RVS Output Voltage	23k from RVS to GND	2.87	3	3.13	V

Note 1: Gain constant (K) = $\dfrac{IAC \cdot (VA_{OUT} - 1.5V)}{(V_{RMS}^2 \cdot IMO)}$ at V_{RMS} = 1.5V, VA_{OUT} = 5.5V.

PIN DESCRIPTIONS

CA−: This is the inverting input to the current amplifier. Connect the required compensation components between this pin and CAOUT. The common mode operating range for this input is between −0.3V and 5V.

CAO: This is the output of the wide bandwidth current amplifier and one of the inputs to the PWM duty cycle comparator. The output signal generated by this amplifier commands the PWM to force the correct input current. The output can swing from 0.1V to 7.5V.

CI: The level shifted current sense signal is impressed upon a capacitor connected between this pin and GND. The buffered current sense transformer signal charges the capacitor when the boost switch is on. When the switch is off, the current synthesizer discharges the capacitor at a rate proportional to the dI/dt of the boost inductor current. In this way, the discharge current is approximately equal to

$$\frac{3V}{RRVS} - \frac{IAC}{4}.$$

Discharging the CI capacitor in this fashion, a "reconstructed" version of the inductor current is generated using only one current sense transformer.

CS: The reconstructed inductor current waveform generated on the CI pin is level shifted down a diode drop to this pin. Connect the current amplifier input resistor between CS and the inverting input of the current amplifier. The waveform on this pin is compared to the multiplier output waveform through the average current sensing current amplifier. The input to the peak current limiting comparator is also connected to this pin. A voltage level greater than 1.5 volts on this pin will trip the comparator and disable the gate driver output.

CT: A capacitor from CT to GND sets the PWM oscillator frequency according to the following equation:

$$f \approx \frac{1}{11200 \cdot CT}.$$

Use a high quality ceramic capacitor with low ESL and ESR for best results. A minimum CT value of 200pF insures good accuracy and less susceptibility to circuit layout parasitics. The oscillator and PWM are designed to provide practical operation to 500kHz.

GND: All voltages are measured with respect to this pin. All bypass and timing capacitors connected to GND should have leads as short and direct as possible.

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PIN DESCRIPTIONS (cont.)

GTOUT: The output of the PWM is a 1.5A peak totem pole MOSFET gate driver on GTOUT. A series resistor between GTOUT and the MOSFET gate of at least 10 ohms should be used to limit the overshoot on GTOUT. In addition, a low V_F Schottky diode should be connected between GTOUT and GND to limit undershoot and possible erratic operation.

IAC: This is a current input to the multiplier. The current into this pin should correspond to the instantaneous value of the rectified AC input line voltage. This is accomplished by connecting a resistor directly between IAC and the rectified input line voltage. The nominal 650mV level present on IAC negates the need for any additional compensating resistors to accommodate for the zero crossings of the line. A current equal to one fourth of the IAC current forms one of the inductor current synthesizer inputs.

IMO: This is the output of the multiplier, and the non-inverting input of the current amplifier. Since this output is a current, connect a resistor between this pin and ground equal in value to the input resistor of the current amplifier. The common mode operating range for this pin is −0.3V to 5V.

ION: This pin is the current sensing input. It should be connected to the secondary side output of a current sensing transformer whose primary winding is in series with the boost switch. The resultant signal applied to this input is buffered and level shifted up a diode to the CI capacitor on the CI pin. The ION buffer has a source only output. Discharge of the CI cap is enabled through the current synthesizer circuitry. The current sense transformer termination resistor should be designed to obtain a 1V input signal amplitude at peak switch current.

OVP: This pin senses the boost output voltage through a voltage divider. The enable comparator input is TTL compatible and can be used as a remote shutdown port. A voltage level below 1.8V, disables V_{REF}, oscillator, and the PWM circuitry via the enable comparator. Between 1.8V and V_{REF} (7.5V) the UC1855 is enabled. Voltage levels above 7.5V will set the PWM latch via the hysteretic OVP comparator and disable both ZVTOUT and GTOUT until the OVP level has decayed by the nominal hysteresis of 400mV. If the voltage divider is designed to initiate an OVP fault at 5% of OV, the internal hysteresis enables normal operation again when the output voltage has reached its nominal regulation level. Both the OVP and enable comparators have direct logical connections to the PWM output and exhibit typical propagation delays of 200ns.

REF: REF is the output of the precision reference. The output is capable of supplying 25mA to peripheral circuitry and is internally short circuit current limited. REF is disabled and low whenever VCC is below the UVLO threshold, and when OVP is below 1.8V. A REF "GOOD" comparator senses REF and disables the stage until REF has attained approximately 90% of its nominal value. Bypass REF to GND with a 0.1μF or larger ceramic capacitor for best stability.

RVS: The nominal 3V signal present on the VSENSE pin is buffered and brought out to the RVS pin. A current proportional to the output voltage is generated by connecting a resistor between this pin and GND. This current forms the second input to the current synthesizer.

VAO: This is the output of the voltage amplifier. At a given input RMS voltage, the voltage on this pin will vary directly with the output load. The output swing is limited from approximately 100mV to 6V. Voltage levels below 1.5V on this pin will inhibit the multiplier output.

VCC: Positive supply rail for the IC. Bypass this pin to GND with a 1μF low ESL, ESR ceramic capacitor. This pin is internally clamped to 20V. Current into this clamp should be limited to less than 10mA. The UC1855A has a 15.5V (nominal) turn on threshold with 6 volts of hysteresis while the UC1855B turns on at 10.5V with 500mV of hysteresis.

VRMS: This pin is the feedforward line voltage compensation input to the multiplier. A voltage on VRMS proportional to the AC input RMS voltage commands the multiplier to alter the current command signal by $1/VRMS^2$ to maintain a constant power balance. The input to VRMS is generally derived from a two pole low pass filter/voltage divider connected to the rectified AC input voltage. This feature allows universal input supply voltage operation and faster response to input line fluctuations for the PFC boost preregulator. For most designs, a voltage level of 1.5V on this pin should correspond to low line, and 4.7V for high line. The input range for this pin extends from 0 to 5.5V.

VSENSE: This pin is the inverting input of the voltage amplifier and serves as the output voltage feedback point for the PFC boost converter. It senses the output voltage through a voltage divider which produces a nominal 3V. The voltage loop compensation is normally connected between this pin and VAO. The VSENSE pin must be above 1.5V at 25°C, (1.9V at −55°C) for the current synthesizer to work properly.

PIN DESCRIPTIONS (cont.)

ZVS: This pin senses when the drain voltage of the main MOSFET switch has reached approximately zero volts, and resets the ZVT latch via the ZVT comparator. A minimum and maximum ZVTOUT pulse width are programmable from this pin. To directly sense the ≈400V drain voltage of the main switch, a blocking diode is connected between ZVS and the high voltage drain. When the drain reaches 0V, the level on ZVS is ≈0.7V which is below the 2.6V ZVT comparator threshold. The maximum ZVTOUT pulse width is approximately equal to the oscillator blanking period time.

For more information see Unitrode Applications Note U-153.

ZVTOUT: The output of the ZVT block is a 750mA peak totem pole MOSFET gate driver on ZVTOUT. Since the ZVT MOSFET switch is typically 3X smaller than the main switch, less peak current is required from this output. Like GTOUT, a series gate resistor and Schottky diode to GND are recommended. This pin may also be used as a high current synchronization output driver.
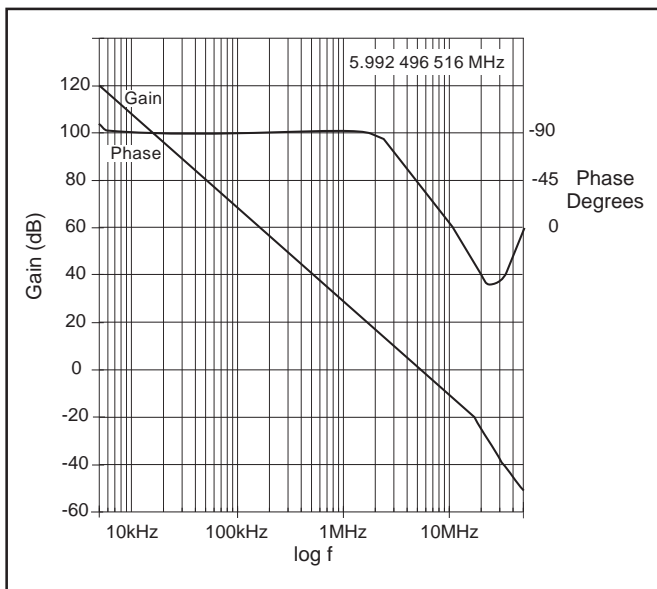
Figure 1. Current Amplifier Frequency Response
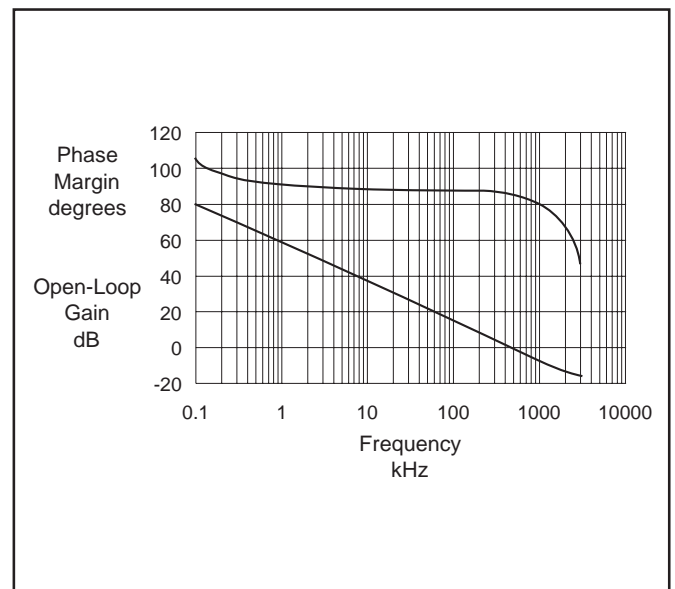
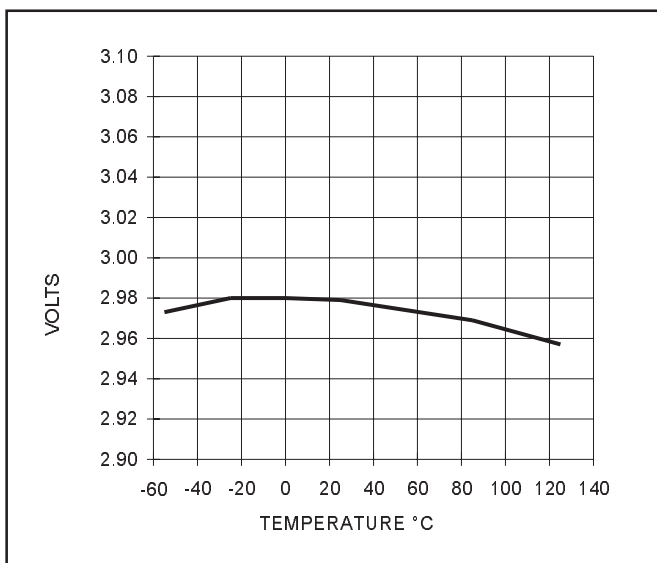*Figure 2. Voltage Amplifier Gain Phase vs Frequency*
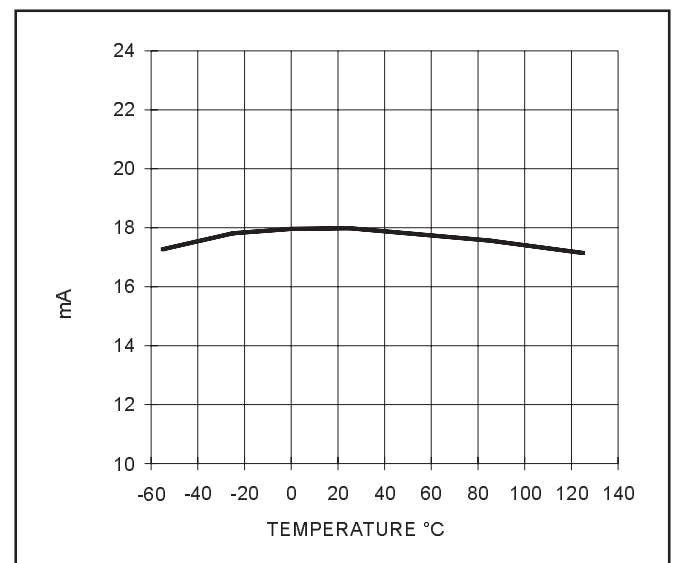

Figure 3. Voltage Amplifier Input Threshold

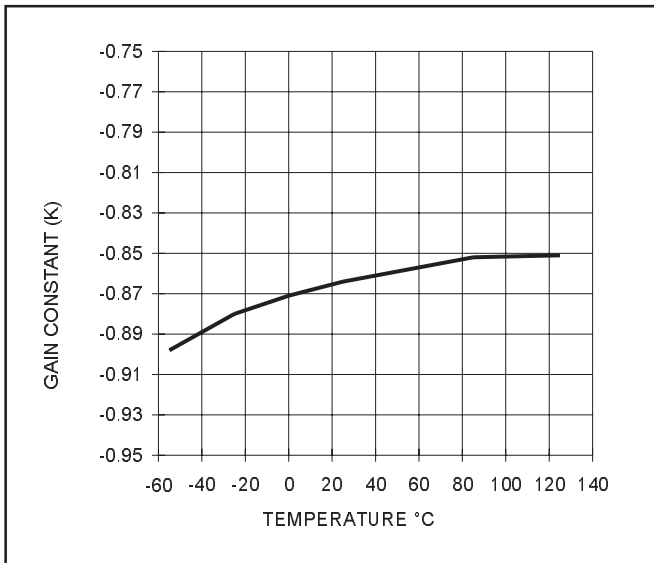*Figure 4. Supply Current ON*

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Figure 5. Multiplier Current Gain Constant
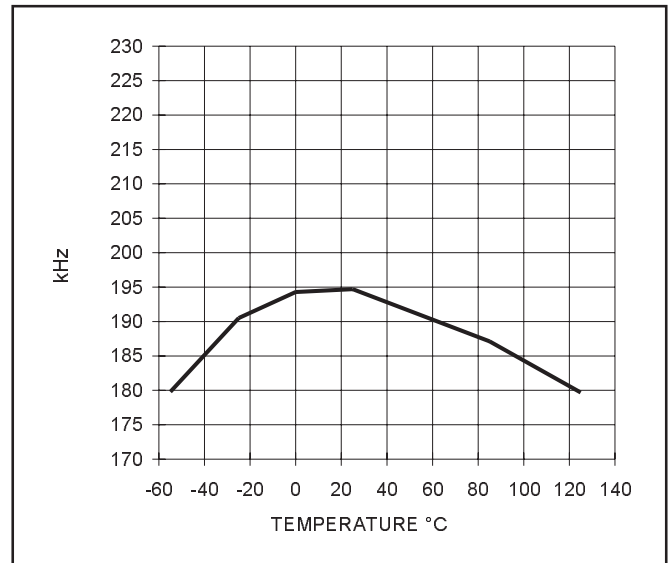
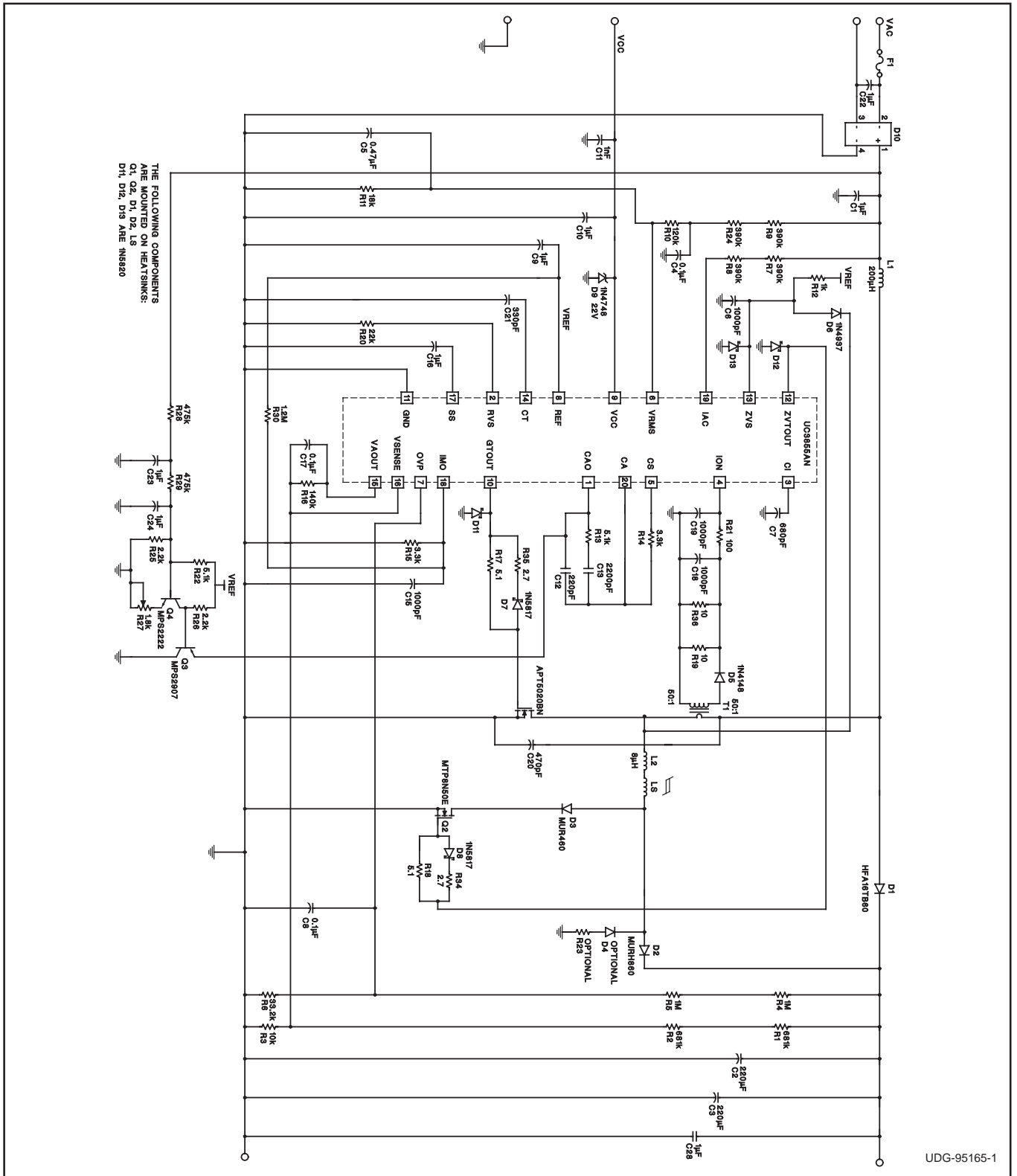**Figure 6. Oscillator Initial Accuracy**

TYPICAL APPLICATION

UDG-95165-1

Figure 7. Typical Application

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